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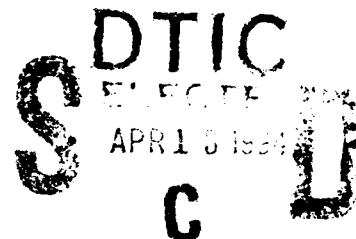
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**SNOWMELT FORECASTING -  
FURTHER COLD REGIONS DEVELOPMENT OF  
OPERATIONAL HYDROLOGICAL FORECASTING**

Volume 2

by

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**PREFACE**

This volume contains all the information that is required to operate the computer simulation model SNOMO. The input files required, the operational logic of SNOMO and the output produced by SNOMO are discussed in detail. A full listing of the SNOMO Fortran-77 code is included.

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## CHAPTER 1: INPUT

### 1.1 Cell division.

The catchment is subdivided into computational units, called cells. The factors used for this subdivision are slope angle, aspect, elevation and vegetation cover type. The method for catchment subdivision is described in detail in chapter 5 (volume 1) and need not be repeated here. The catchment to be modelled will therefore consist of, after subdivision, a number of cells each with an aspect, slope angle, elevation and vegetation cover value. The location of each cell in the catchment is also known. The depth and occurrence of snowcover is calculated for each cell and the results for all the cells are examined together in order to calculate the snowcover depth and distribution over the whole catchment.

### 1.2 Input files.

The snowcover calculations are conducted separately for each cell. The presence of five data files (*snomo.dat*, *conif.dat*, *decid.dat*, *mix.dat* and *lapse.dat*) is required in order for SNOMO to operate correctly. The input required for these 5 files will be considered in detail below and has also been discussed in chapter 4 (volume 1).

#### 1.2.1 *snomo.dat*.

Tables 1.1, 1.2 and 1.3 show sample *snomo.dat* files for cells 1 and 24 in 1988 and cell 1 in 1989 for the W3 catchment, Sleepers River Research Watershed, Danville, Vermont. Table 1.4 shows the variables contained in *snomo.dat*. The variables are considered in detail below in the order that they appear in the data file.

**Table 1.1. Sample snomo.dat file for cell 1, W3, 1988.**

1	1	1988				
2	0.0	0.06	0.03	0.99	0.95	0.136
3	0.0	0.24	0.08	0.94	0.40	0.410
4	0.0	0.36	0.09	0.92	0.39	1.600
5	1010	5	100			
6	6.15	-92.83	64	44.47		
7	1					
8	3					
9	69.0					
10	5.0					
11	100.0	0.0	-1.0			
12	39					
13	64	1100	-11.1	-2.8	71.00	0.5 0.7 0.0
14	65	1100	-16.3	-5.8	36.00	0.5 4.2 0.2
15	66	1100	-16.6	0.0	31.00	0.5 1.7 0.0
16	67	1100	-6.0	5.6	46.00	0.7 2.5 1.5
17	68	1100	-14.0	4.4	32.00	0.0 1.7 0.1
18	69	1100	-1.9	4.6	55.00	1.0 1.8 6.1
19	70	1100	-7.8	2.4	75.00	0.5 3.1 1.6
20	71	1100	-15.3	-7.8	42.00	0.0 3.4 1.0
21	72	1100	-16.9	-1.6	37.00	0.5 2.0 0.0
22	73	1100	-3.8	3.6	80.00	0.5 1.1 4.8
23	74	1100	-5.9	0.3	77.00	1.0 1.9 1.4
24	75	1100	-6.2	-2.1	73.00	0.5 2.2 1.2
25	76	1100	-6.5	0.0	68.00	0.7 1.9 2.0
26	77	1100	-10.9	2.7	36.00	0.5 2.5 0.1
27	78	1100	-9.7	2.8	43.00	1.0 1.2 0.0
28	79	1100	-15.3	0.3	46.00	0.5 2.8 0.5
29	80	1100	-19.0	-6.1	67.00	0.5 2.5 2.8
30	81	1100	-22.7	-14.9	51.00	0.4 3.6 0.5
31	82	1100	-19.1	-4.2	46.00	0.5 2.8 0.0
32	83	1100	-15.4	4.8	32.00	0.4 2.7 0.0
33	84	1100	-0.3	11.0	65.00	0.5 1.2 0.0
34	85	1100	-0.4	7.2	81.00	0.5 1.4 0.0
35	86	1100	4.4	7.9	92.00	0.5 0.8 20.7
36	87	1100	-2.2	4.8	92.00	0.5 3.5 10.7
37	88	1100	-6.1	-0.2	78.00	0.5 2.1 1.2
38	89	1100	-8.0	12.7	43.00	0.5 1.1 0.0
39	90	1100	1.8	13.5	31.00	0.0 2.1 0.0
40	91	1100	0.3	10.8	80.00	0.0 2.1 0.0
41	92	1100	0.3	11.0	38.00	0.3 2.2 0.0
42	93	1100	1.1	18.8	47.00	0.5 1.4 0.0
43	94	1100	4.5	8.5	88.00	0.5 1.4 0.2
44	95	1100	3.3	11.8	95.00	1.0 0.5 0.4
45	96	1100	3.3	9.4	95.00	1.0 1.4 16.3
46	97	1100	0.9	15.3	74.00	0.6 1.0 0.0

continued overleaf...

```

47 98 1100 0.3 12.9 61.00 0.5 1.0 0.0
48 99 1100 3.4 6.9 87.00 1.0 1.1 0.5
49 100 1100 1.0 8.7 45.00 0.5 2.9 0.5
50 101 1100 -0.3 6.7 82.00 0.0 3.2 0.0
51 102 1100 -0.7 8.0 76.00 0.5 1.8 1.2
52 103 1100 -0.5 12.5 53.00 0.5 1.2 0.0

```

**Interpretation of snomo.dat file:**

LINE 1 cell identification number, simulation year.

LINE 2 0.0, thermal diffusivity ( $\text{cm}^2 \text{min}^{-1}$ ), heat conductivity ( $\text{cal cm}^{-2} \text{min}^{-1} \text{K}^{-1}$ ), emissivity (decimal), albedo (decimal), density ( $\text{gm}^{-3}$ ): for new snow.

LINE 3 as line 2, but for old snow.

LINE 4 as line 2 and 3, but for sandy soil.

LINE 5 air pressure (mb), cloud type, instrument height (cm).

LINE 6 slope angle, aspect, start date, latitude.

LINE 7 lapse rate indicator.

LINE 8 vegetation cover type indicator.

LINE 9 initial snowdepth, (cm).

LINE 10 critical snowdepth (5cm).

LINE 11 depth of soil profile (cm), soil temperature at depth ( $^{\circ}\text{C}$ ), surface soil temperature ( $^{\circ}\text{C}$ ).

LINE 12 number of days in data file minus one.

LINE 13 daily meteorological data: Julian date, observation time, minimum air temperature ( $^{\circ}\text{C}$ ), maximum air temperature ( $^{\circ}\text{C}$ ),

TO 52 relative humidity (%), cloud cover (0-1), wind speed ( $\text{ms}^{-2}$ ).

Table 1.2. Sample *snomo.dat* file for cell 24, W3, 1988.

```
1 24 1988
2 0.0 0.06 0.03 0.99 0.95 0.136
3 0.0 0.24 0.08 0.94 0.40 0.410
4 0.0 0.36 0.08 0.92 0.39 1.600
5 1010 5 100
6 6.27 -101.37 64 44.47
7 0
8 0
9 69.0
10 5.0
11 100.0 0.0 -1.0
12 39
13 64 1100 -11.1 -2.8 71.00 0.5 0.7 0.0
Lines 14 to 52 as file (1).
```

Table 1.3. Sample *snomo.dat* file for cell 1, W3, 1989.

```

1 1 1989
2 0.0 0.06 0.03 0.99 0.95 0.136
3 0.0 0.24 0.08 0.94 0.40 0.410
4 0.0 0.36 0.09 0.92 0.39 1.600
5 1010 5 100
6 6.15 -92.83 64 44.47
7 1
8 3
9 52.9
10 5.0
11 100.0 0.0 -1.0
12 46
13 64 1100 -8.5 0.7 96.00 0.5 0.3 7.1
14 65 1100 -19.9 -9.4 81.00 1.0 2.5 0.0
15 66 1100 -28.7 -15.8 65.00 0.5 1.7 0.0
16 67 1100 -20.4 -5.9 72.00 0.0 1.3 0.0
17 68 1100 -14.9 -1.2 67.00 0.0 1.4 0.0
18 69 1100 -11.5 1.8 52.00 0.5 1.7 0.0
19 70 1100 -7.6 2.02 47.00 0.5 1.9 1.02
20 71 1100 -12.6 -1.7 87.00 0.5 2.4 1.8
21 72 1100 -16.0 -1.3 40.00 0.0 1.2 0.0
22 73 1100 -3.9 8.6 61.00 0.5 1.0 0.0
23 74 1100 3.4 14.3 96.00 0.5 1.8 0.0
24 75 1100 -4.6 2.5 78.00 0.5 2.2 0.0
25 76 1100 -6.7 2.6 75.00 1.0 2.1 3.1
26 77 1100 -8.1 1.0 97.00 0.5 0.4 17.0
27 78 1100 -12.5 -6.1 84.00 0.5 1.7 1.02
28 79 1100 -12.1 -0.6 87.00 1.0 1.2 1.52
29 80 1100 -9.3 -0.9 94.00 0.5 2.0 7.6
30 81 1100 -14.3 -3.6 57.00 0.5 1.8 0.0
31 82 1100 -10.7 2.6 47.00 0.0 1.8 0.0
32 83 1100 -9.4 2.2 55.00 0.5 1.8 2.5
33 84 1100 -2.7 6.3 89.00 0.5 0.8 3.1
34 85 1100 0.0 6.5 91.00 0.5 1.1 0.0
35 86 1100 0.0 16.9 60.00 0.5 0.9 0.0
36 87 1100 7.0 17.1 79.00 0.2 0.8 2.3
37 88 1100 -0.2 13.8 65.00 1.0 1.7 13.5
38 89 1100 -2.4 0.4 93.00 0.5 1.2 18.3
39 90 1100 -2.7 0.3 97.00 1.0 0.6 10.2
40 91 1100 -2.3 0.2 94.00 0.5 1.8 4.3
41 92 1100 -3.4 6.5 83.00 0.5 1.3 0.0
42 93 1100 1.0 3.8 94.00 1.0 1.1 26.2
43 94 1100 1.2 4.6 99.00 1.0 0.8 6.9
44 95 1100 4.3 14.0 90.00 0.4 0.9 8.4
45 96 1100 0.1 6.5 98.00 0.5 1.9 21.3
46 97 1100 0.1 4.2 94.00 0.6 1.7 9.4

```

continued overleaf...

47	98	1100	-3.4	2.6	82.00	0.5	2.4	0.0
48	99	1100	-4.8	6.2	43.00	0.5	1.3	3.1
48	100	1100	-5.7	1.2	70.00	0.5	1.6	6.6
50	101	1100	-7.9	-0.2	70.00	0.7	1.7	0.0
51	102	1100	-7.1	4.2	66.00	0.5	0.7	0.0
52	103	1100	-1.1	5.8	58.00	0.5	1.9	0.0
53	104	1100	-0.3	5.2	73.00	0.9	1.1	0.0
54	105	1100	0.4	6.8	71.00	0.5	2.1	6.4
55	106	1100	1.0	4.6	97.00	0.5	0.9	4.6
56	107	1100	3.5	14.7	80.00	0.5	0.8	0.0
57	108	1100	0.4	11.1	95.00	0.5	2.4	3.8
58	109	1100	-0.8	5.9	53.00	0.5	1.9	0.0
59	110	1100	-0.6	5.2	90.00	0.5	2.1	1.8

Table 1.4. Description of variables in *snomo.dat*.

LINE	VARIABLE	REAL/ INTEGER	DESCRIPTION
1	CELL	I	Number of cell.
	YEAR	I	Year of simulation
2	VNEWSN(1,1)	R	New snow vector, 0.0.
	VNEWSN(1,2)	R	" " " , thermal diffusivity ( $\text{cm}^2 \text{min}^{-1}$ ).
	VNEWSN(1,3)	R	" " " , heat conductivity ( $\text{calcm}^{-2} \text{min}^{-1} \cdot \text{K}^{-1}$ ).
	VNEWSN(1,4)	R	" " " , emissivity (decimal).
	VNEWSN(1,5)	R	" " " , albedo (decimal).
	VNEWSN(1,6)	R	" " " , density ( $\text{gcm}^{-3}$ ).
3	VOLDSN(1,1)	R	Old snow vector, 0.0.
	VOLDSN(1,2)	R	" " " , thermal diffusivity ( $\text{cm}^2 \text{min}^{-1}$ ).
	VOLDSN(1,3)	R	" " " , heat conductivity ( $\text{calcm}^{-2} \text{min}^{-1} \cdot \text{K}^{-1}$ ).
	VOLDSN(1,4)	R	" " " , emissivity (decimal).
	VOLDSN(1,5)	R	" " " , albedo (decimal).
	VOLDSN(1,6)	R	" " " , density ( $\text{gcm}^{-3}$ ).
4	VSOIL(1,1)	R	Soil vector, 0.0.
	VSOIL(1,2)	R	" " , thermal diffusivity ( $\text{cm}^2 \text{min}^{-1}$ ).
	VSOIL(1,3)	R	" " , heat conductivity ( $\text{calcm}^{-2} \text{min}^{-1} \cdot \text{K}^{-1}$ ).
	VSOIL(1,4)	R	" " , emissivity (decimal).
	VSOIL(1,5)	R	" " , albedo (decimal).
	VSOIL(1,6)	R	" " , density ( $\text{gcm}^{-3}$ ).
5	PRESS	I	Air pressure (mb).
	NCLOUD	I	Cloud type, see table 1.2.
	ZA	I	Instrument height (cm).
6	SLOPE1	R	Cell slope angle (°)
	SURFC1	R	Cell aspect (°)
	DAY1	I	Start date (Julian calendar).
	LAT	R	Latitude of catchment (°).
7	ILAPSE	I	Lapse rate indicator. ILAPSE=0, elevation band 1500-2000ft. ILAPSE=1, elevation band 1000-1500ft.
8	IVEG	I	Cell vegetation cover type indicator. IVEG=1, coniferous cover. IVEG=2, deciduous cover. IVEG=3, mixed cover. IVEG=0, pasture and clear-cut (open).

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9	SNDP1	R	Initial snowdepth (cm).
10	CRI	R	Critical snowdepth (5cm).
11	SOILDp	R	Depth of soil profile (cm).
	SOILTp	R	Soil temperature at depth ( $^{\circ}$ C).
	SSOLTp	R	Surface soil temperature ( $^{\circ}$ C).
12	N	I	Number of days to be modelled. Number of daily meteorological data days minus 1.
13			Daily meteorological data.
	XXX(1,8)	I	Date (Julian calendar).
	XXX(1,1)	I	Observation time (24hr clock).
	YYY(1,1)	R	Minimum daily air temperature ( $^{\circ}$ C).
	YYY(1,9)	R	Maximum daily air temperature ( $^{\circ}$ C).
	YYY(1,2)	R	Relative humidity (%)
	YYY(1,3)	I	Cloud cover (0-1).
	YYY(1,6)	R	Wind speed ( $m s^{-1}$ ).
	YYY(1,7)	R	Precipitation (mm water).

LINE 1

## 1. CELL

The number of the cell. Each cell is numbered for easy identification.

## 2. YEAR

The year of the simulation.

LINE 2: 'New' snow vector.

The vector for the physical characteristics of 'new' snow. Chapter 4 (volume 1) considered the division of the physical characteristics of snow into those commonly associated with 'new' (fresh) snow and 'old' snow. Values are taken from various sources or measurements on site if available. The physical characteristics required are thermal diffusivity ( $\text{cm}^2\text{min}^{-1}$ ), heat conductivity ( $\text{calcm}^{-2}\text{min}^{-1}\cdot\text{K}^{-1}$ ), emissivity (decimal), albedo (decimal) and density ( $\text{gcm}^{-3}$ ). The first value in the vector is always input as zero. This is because it represents snowpack depth and is calculated within the program.

LINE 3: 'Old' snow vector.

As line 2, except concerned with the values of the physical characteristics of 'old' snow.

LINE 4: Soil vector.

As lines 2 and 3, except concerned with the values of the physical characteristics of the soil. Soil type is taken as the predominant soil type for that particular cell or catchment. The soil vector is rarely used and therefore the accuracy of the soil values is not particularly important. Again values can be taken from the literature, or on site.

LINE 5

## 1. PRESS.

Air pressure (mb). The average air pressure for the simulation period is used, or a median value.

## 2. NCLOUD.

Values for cloud cover type are contained in table 1.5. The average cloud cover type is used or, in the absence of sufficient data, a default cloud cover type of 5 (stratocumulus) is used.

## 3. ZA.

Instrument height is the average height (cm) of the instruments used to measure the meteorological data, ie. wind speed and relative humidity, from the ground/snow surface. If this measurement is unavailable or is too variable a default value of 100cm is used.

LINE 6

## 1. SLOPE1.

Cell slope angle (°).

## 2. SURFC1.

Cell aspect. The cell aspect is measured in degrees from South with westerly values positive and easterly values negative, ie. West=+90° and East=-90°.

## 3. DAY1.

Date of start of simulation, Julian calender.

## 4. LAT.

Latitude of catchment or cell (degrees and minutes). The latitude of the midpoint or mouth of the catchment can be used, at the operator's discretion.

LINE 7

## 1. ILAPSE.

Lapse rate indicator. SNOMO is currently set up for the W3 catchment, Sleepers River Research Watershed, Danville, Vermont. When subdivided the elevations derived for each cell ranged within 1000-2000ft a.s.l.. A midpoint of 1500ft a.s.l. was used as a

**Table 1.5. Cloud Genera and Cloud Type Indices<sup>\*</sup>, Balick *et.al.* (1981a).**

Cloud Genera	Abbreviation	Index value	Comments
Cirrus	Ci	1	High clouds composed of white delicate filaments, patches of narrow bands, elements often curved or slanted and smaller than Cs, never overcast or precipitating.
Cirrostratus	Cs	2	High clouds appearing as whitish veil usually fibrous, often produces halo phenomena, thinner than As, does not appear to move, nonprecipitating.
Altocumulus	Ac	3	Midlevel clouds, patches, usually broken, less wave clouds, elements smaller than Sc, nonprecipitating.
Altostratus	As	4	Midlevel grey sheet or layer of striated, fibrous or uniform appearance, large horizontal extent; thicker than Cs, thinner thanNs, precipitation generally light and continuous (if any).
Stratocumulus	Sc	5	Grey and/or whitish layer or patch, nearly always has dark spots and is nonfibrous; elements larger than Ac, nonprecipitating.
Stratus	St	6	Grey rather uniform base, patches ragged if present, precipitation unusual but light and continuous if present, lower and more uniform than Sc, less dense and less 'wet' than Ns.
Nimbostratus	Ns	7	Grey often dark, diffuse, large horizontal and vertical extent, thicker than As, more uniform than Sc, often precipitating, precipitation continuous.
Fog	FG	8	

\* Cloud genera; Cumulus (Cu), Cirrocumulus (Cc) and Cumulonimbus (Cb) are not treated here. At low cloud covers (0.3) Cu and Cc may be approximated with Ac.

further subdivision of the elevation resulting in 2 elevation bands: 1000-1500ft and 1500-2000ft. If the elevation of the cell is between 1000-1500ft the lapse rate indicator is set to 1, if between 1500-2000 then it is set to 0. The elevation bands can be altered if required.

#### LINE 8

##### 1. IVEG.

Vegetation cover type indicator. Four vegetation cover types can be modelled using SNOMO:

IVEG=1, coniferous cover

IVEG=2, deciduous cover

IVEG=3, mixed cover

IVEG=0, pasture or clear-cut (open).

The vegetation cover types are those found at W3. Again, as with ILAPSE, these can be altered if necessary.

#### LINE 9

##### 1. SNDP1.

Initial snowdepth. This is the known (measured or estimated) snowdepth for the cell at the start of the simulation. If estimated the value for initial snowdepth is based on the relationship between snowdepth, vegetation cover type and elevation. If one value at a base station (1500-2000ft a.s.l) is available then:

- (1) Cell with elevation < 1500ft a.s.l., -10cm.
- (2) Cell with coniferous forest cover, -5cm.
- (3) Cell with mixed forest cover, +5cm.
- (4) Cell with deciduous forest cover, +10cm.

These values can be used or compiled according to another catchment.

#### LINE 10

##### 1. CRITDP.

Critical depth (5cm). This is the depth below which, because of the difficulty of accurate measurement, no snow is said to be

present.

LINE 11

1. SOILDP.

Depth of soil profile (cm). Default value is 100cm.

2. SOILTP.

Soil temperature at depth ( $^{\circ}$ C). Default value is  $0^{\circ}$ C. SNOMO does not currently model the temperatures within the soil or the heat flux across the ground/snow interface ( $Q_g$ ) and therefore the accuracy of SOILTP is not vital.

3. SSOLTP.

Surface soil temperature ( $^{\circ}$ C). Default value of  $-1^{\circ}$ C is used. Again, for the same reasons as SOILTP, accuracy is not vital.

LINE 12

1. N

The number of days to be modelled in the simulation. This is calculated as the number of daily meteorological data available in *snomo.dat* minus one.

LINE 13 and onward : Daily meteorological data.

1. XXX(1,8)

Julian date.

2. XXX(1,1)

Observation time (24hr clock), default value of 1100hrs.

3. YYY(1,1)

Minimum air temperature ( $^{\circ}$ C).

4. YYY(1,9)

Maximum air temperature ( $^{\circ}$ C).

5. YYY(1,2)

Relative humidity (%).

6. YYY(1,3)

Cloud cover amount (decimal).

7. YYY(1,6)

Wind speed ( $\text{ms}^{-1}$ )

8. YYY(1,7)

Precipitation (mm water).

Table 1.6 is provided for the guidance of the compilation of a snomo.dat file.

#### 1.2.2 conif.dat, decid.dat and mix.dat.

These three data files contain the information required if the vegetation cover options of coniferous, deciduous or mixed cover are used. The files contain values of the variables  $\sigma_f$ ,  $x$ ,  $\epsilon_f$ ,  $\alpha_f$  and  $z_f$ . Examples of the three data files used for the W3 simulation are shown in table 1.7. The variables contained in the files are considered in chapter 4 (volume 1) and below:

##### 1. $\sigma_f$ , foliage cover fraction (0-1).

This describes the density of the vegetation cover.  $\sigma_f=0$  represents no foliage and therefore no radiative shielding and  $\sigma_f=1$  represents complete radiative blocking. Table 1.4 shows various limiting values of  $\sigma_f$  taken from Geiger (1965) and Deardorff (1978) for various vegetation covers.

##### 2. $x$ , state of vegetation (1-1000).

$x$  is used as a multiplier of the stomatal resistance function. A summer value, when the vegetation is healthy and active, is 1, a winter and therefore dominant or dead vegetation cover value is 1000. Other values can be chosen to adjust stomatal resistance for moisture stress, senescence or other factors.

##### 3. $\epsilon_f$ , foliage emissivity (decimal).

##### 4. $\alpha_f$ , foliage albedo (decimal).

##### 5. $z_f$ , foliage height (cm).

Values for  $\epsilon_f$  and  $\alpha_f$  can be obtained from the literature.

**Table 1.6.** Compilation guideline for *snomo.dat*.

All input on the same line is separated by at least 1 space and starts in the first column.

**LINE 1**

1. Number of cell	_____
2. Year of simulation	_____

**LINE 2**

1. 0.0	<u>0.0</u>
2. New snow thermal diffusivity	_____
3. " " heat conductivity	_____
4. " " emissivity	_____
5. " " albedo	_____
6. " " density	_____

**LINE 3**

1. 0.0	<u>0.0</u>
2. Old snow thermal diffusivity	_____
3. " " heat conductivity	_____
4. " " emissivity	_____
5. " " albedo	_____
6. " " density	_____

**LINE 4**

1. 0.0	<u>0.0</u>
2. Soil thermal diffusivity	_____
3. " heat conductivity	_____
4. " emissivity	_____
5. " albedo	_____
6. " density	_____

continued overleaf...

## LINE 5

1. Air pressure

---

2. Cloud type

---

3. Instrument height

---

## LINE 6

1. Cell slope angle

---

2. Cell aspect

---

3. Start date

---

4. Latitude of catchment or cell

---

## LINE 7

1. Lapse rate indicator

---

## LINE 8

1. Cell vegetation cover type indicator

---

## LINE 9

1. Initial snowdepth

---

## LINE 10

1. Critical snowdepth

---

## LINE 11

1. Depth of soil profile

---

2. Soil temperature at depth

---

3. Surface soil temperature

---

## LINE 12

1. Number of days to be modelled

---

continued overleaf...

**LINE 13**

1. Julian date	_____
2. Observation time	_____
3. Minimum daily air temperature	_____
4. Maximum daily air temperature	_____
5. Relative humidity	_____
6. Cloud cover amount	_____
7. Wind speed	_____
6. Precipitation	_____

Table 1.7. *conif.dat*, *decid.dat* and *mix.dat* files used for W3.

*conif.dat*: 0.70,1000,0.98,0.10,2000

*decid.dat*: 0.50,1000,0.97,0.15,2000

*mix.dat*: 0.60,1000,0.975,0.125,2000

**Interpretation:**

1.  $\sigma_f$ , foliage cover fraction (0-1)
2.  $x$ , state of vegetation (1-1000)
3.  $\epsilon_f$ , foliage emissivity (decimal)
4.  $\alpha_f$ , foliage albedo (decimal)
5.  $z_f$ , foliage height (cm).

Table 1.8. *lapse.dat* file used for W3.

*lapse.dat*: 2.0,1.0

**Interpretation:**

1. TMAX, lapse rate factor for daily maximum temperature ( $^{\circ}\text{C}$ ).
2. TMIN, lapse rate factor for daily minimum temperature ( $^{\circ}\text{C}$ ).

### 1.2.3 *lapse.dat*.

The file *lapse.dat* contains values for TMAX and TMIN. These are the lapse rate alteration of the maximum (TMAX) and minimum (TMIN) daily air temperatures. The values for the lapse rate alteration are those used for the catchment W3 and are obtained from the literature (chapters 4 and 6, volume 1). If applied to different catchments the values can be altered if necessary. An example of the *lapse.dat* file used for the W3 simulation is shown in table 1.8.

**CHAPTER 2: OUTPUT****2.1 Output file.**

Table 2.1 shows the output file SNOMO.RES for cell 1, W3, 1988. The input file used was that shown in table 1.1. The output variables are considered below in the order in which they appear in SNOMO.RES and using the titles used in SNOMO.RES.

**1. CELL NO.**

The identification number of the cell.

**2. YEAR**

The year of the simulation.

**3. JULIAN DATE**

Date, Julian calendar.

**4. SNOWDEPTH**

Calculated depth of snowpack (cm).

**5. SNOWMELT**

Calculated daily depth of snow melted, in both centimetres of snow and millimetres of water equivalent.

**6. SNOWFALL**

Daily snowfall (mm water equivalent). The value for snowfall on the first day of simulation is equal to the initial snowpack depth and is not related to the amount of daily snowfall.

**7. DENSITY**

Daily average snowpack density ( $\text{g cm}^{-3}$ ).

**8. RAIN-ON-SNOW**

Occurrence of a rain-on-snow event. 1-rain-on-snow event, 0-no rain-on-snow event.

Table 2.1. Sample SNOMO.RES file, for cell 1, W3, 1988

CELL NO.: 1

YEAR: 1988

JULIAN	SNOWDEPTH (cm)	SNOWMELT (cm snow)	(mm water)	SNOWFALL (cm)	DENSITY (g/m^3)	RAIN-ON-SNOW (1=yes, 0=no)
64.00	69.00	0.00	0.00	69.00	0.39	0
65.00	69.15	0.00	0.00	0.15	0.39	0
66.00	69.15	0.00	0.00	0.00	0.39	0
67.00	66.81	0.00	0.00	1.10	0.39	0
68.00	66.88	0.00	0.00	0.07	0.41	0
69.00	71.37	0.00	0.00	4.49	0.41	0
70.00	72.55	0.00	0.00	1.18	0.39	0
71.00	73.28	0.00	0.00	0.74	0.38	0
72.00	73.28	0.00	0.00	0.00	0.38	0
73.00	71.75	0.00	0.00	3.53	0.38	0
74.00	72.78	0.00	0.00	1.03	0.40	0
75.00	73.66	0.00	0.00	0.88	0.39	0
76.00	75.13	0.00	0.00	1.47	0.39	0
77.00	75.29	0.00	0.00	0.07	0.38	0
78.00	75.20	0.00	0.00	0.00	0.38	0
79.00	70.80	0.00	0.00	0.37	0.38	0
80.00	67.05	5.91	24.24	2.06	0.41	0
81.00	61.97	5.45	22.34	0.37	0.41	0
82.00	60.20	1.77	7.26	0.00	0.41	0
83.00	60.20	0.00	0.00	0.00	0.41	0
84.00	58.35	1.85	7.60	0.00	0.41	0
85.00	55.32	3.03	12.42	0.00	0.41	0
86.00	50.89	4.43	18.14	0.00	0.41	1
87.00	54.10	4.66	19.13	7.87	0.41	0
88.00	54.98	0.00	0.00	0.88	0.39	0
89.00	54.98	0.00	0.00	0.00	0.39	0
90.00	52.25	0.00	0.00	0.00	0.39	0
91.00	47.58	4.67	19.14	0.00	0.41	0
92.00	43.43	4.16	17.04	0.00	0.41	0
93.00	38.68	4.75	19.46	0.00	0.41	0
94.00	34.08	4.60	18.85	0.00	0.41	1
95.00	30.26	3.83	15.69	0.00	0.41	1
96.00	25.42	4.84	19.83	0.00	0.41	1
97.00	19.96	5.46	22.38	0.00	0.41	0
98.00	14.72	5.24	21.49	0.00	0.41	0
99.00	9.87	4.85	19.88	0.00	0.41	1
100.00	4.00	5.88	24.10	0.00	0.41	1

## CHAPTER 3: PROGRAMME DETAILS

### 3.1. Programme structure.

Chapter 4, volume 1, considers in detail the equations used by SNOMO to calculate snowdepth within one cell. This chapter presents the programme logic that enables these equations to be utilised and to interact successfully. Figure 3.1 shows the SNOMO programme logic. SNOMO broadly consists of 2 sections:

#### (1) Control programme.

This is responsible for the determination of the type of precipitation, the calculation of melt, the calculation of the effect of a rain-on-snow event, the calculation of the heat flux across the ground/snow interface ( $Q_g$ ), various operational markers, the calculation of the depth of the snowpack and the physical characteristics of the snowpack, the model input and the model output.

#### (2) Algorithm to calculate the majority of the components of the snowpack energy budget.

This algorithm is responsible for the calculation of the snowpack energy budget components  $K_t$ ,  $K_{\downarrow}$ ,  $L_t$ ,  $L_{\downarrow}$ ,  $Q_c$  and  $Q_e$  and the snowpack surface and internal temperatures. The algorithm is adapted from the US Corps of Engineers Terrain surface Temperature Model (TSTM) as developed by Balick *et.al.* (1981a & b). The basic equations used by the original TSTM remain the same as in the modified TSTM. TSTM has been heavily modified from its original state as presented in Balick *et.al.* (1981a & b) and has also been incorporated into the logic structure of SNOMO. The logic structure of TSTM is shown in figure 3.2. TSTM is operational for situations where a vegetation cover is present or absent. Vegetation cover is modelled using a vegetation cover algorithm, VEGIE, within TSTM.

The relationship between TSTM and VEGIE is shown in figure 3.3.

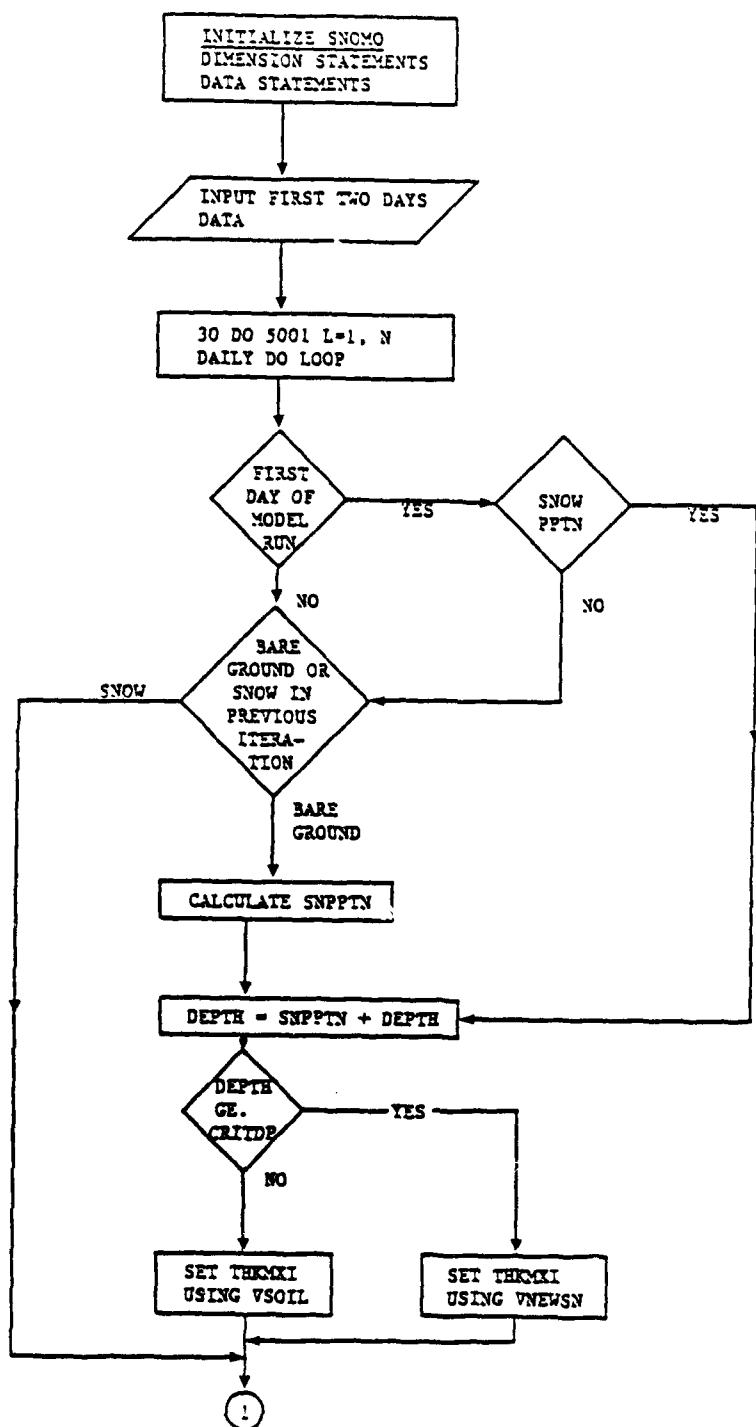


Figure 3.1. Simplified flowchart for SNOMO (sheet 1 of 4).

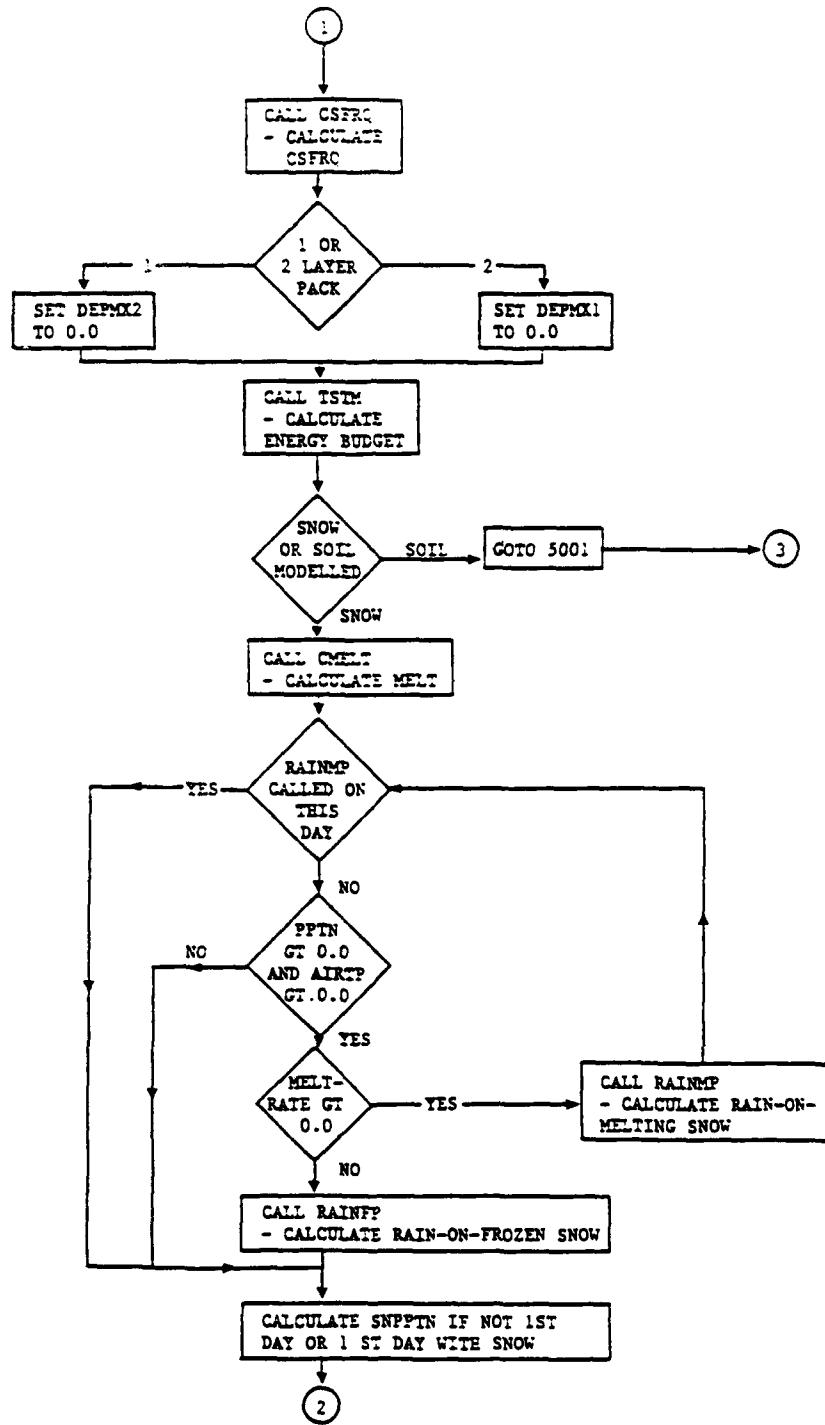


Figure 3.1. Simplified flowchart for SNOMO (sheet 2 of 4).

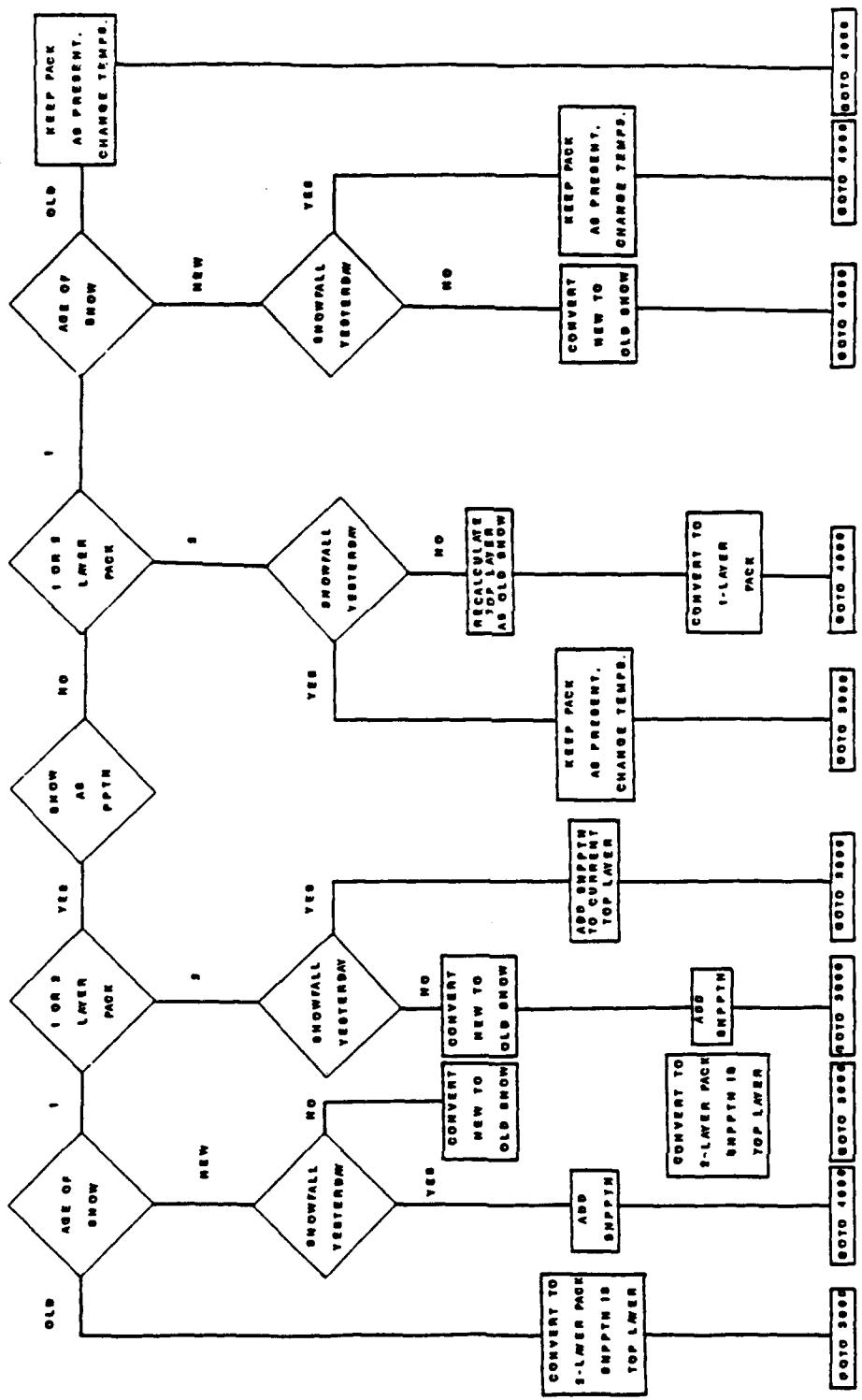


Figure 3.1. Simplified flowchart for SNOMO (sheet 3 of 4).

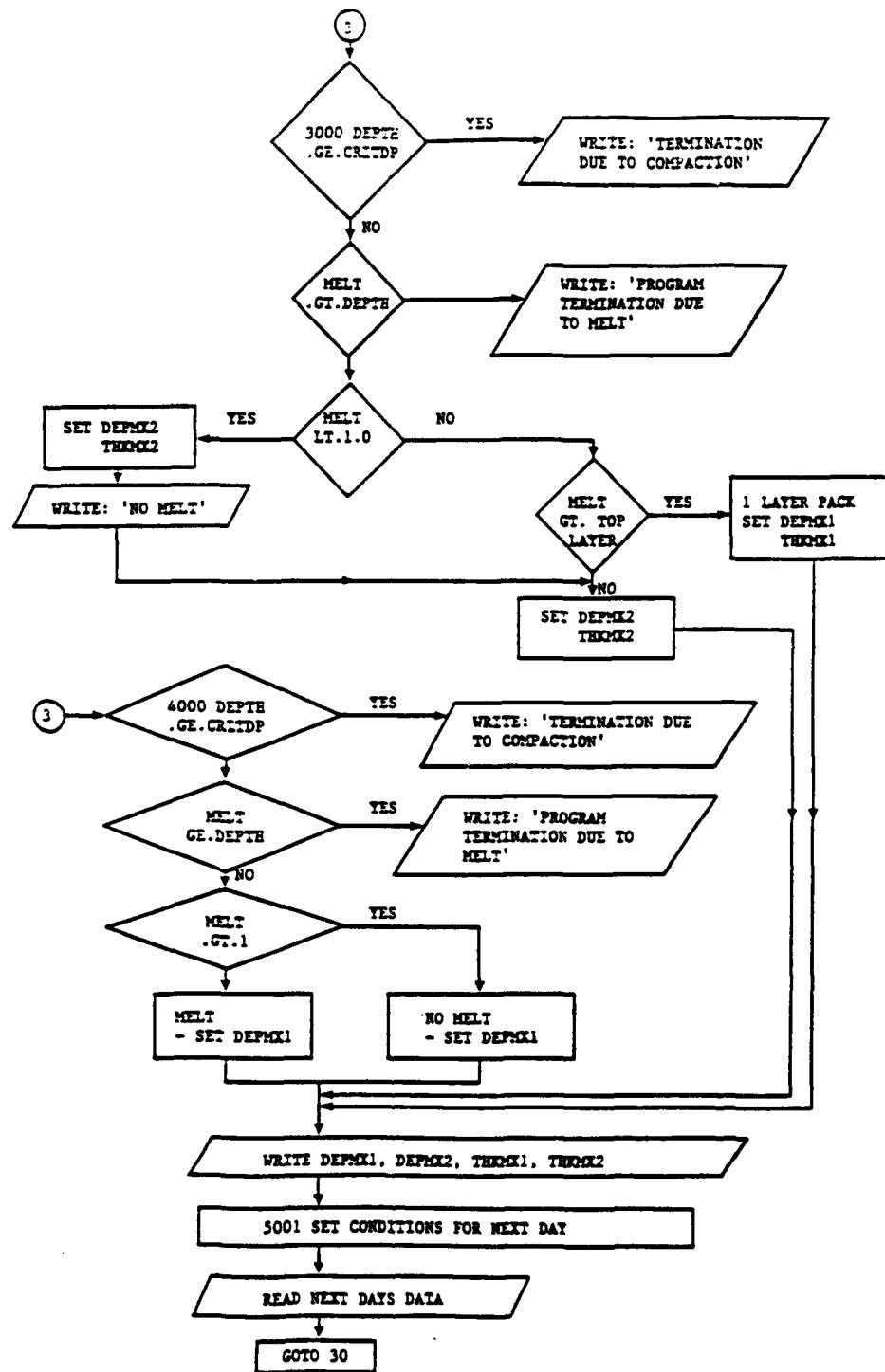


Figure 3.1. Simplified flowchart for SNOMO (sheet 4 of 4).

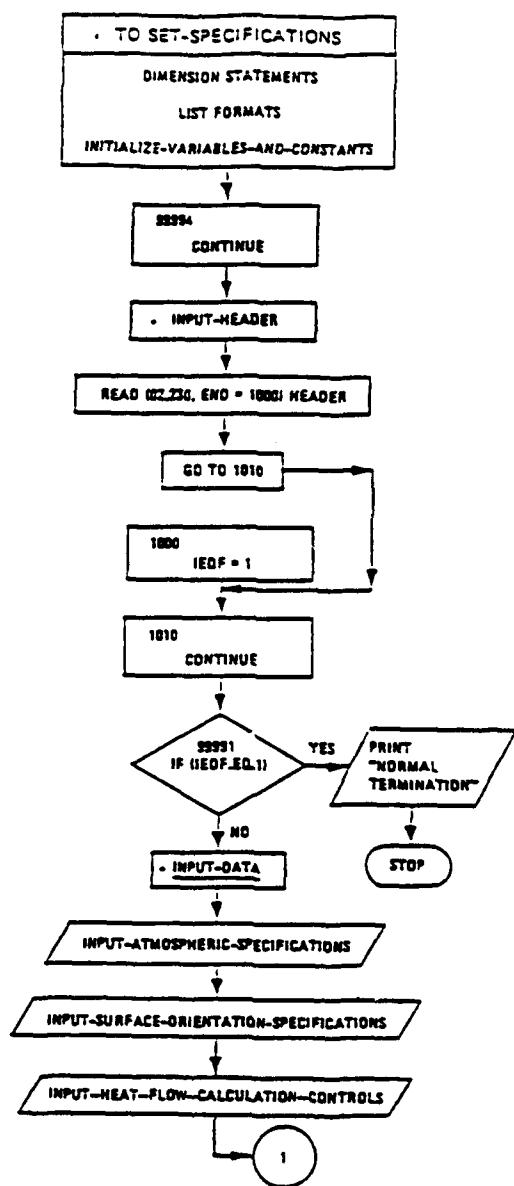


Figure 3.2. Simplified flowchart for TSTM, Balick et al., 1981a  
(sheet 1 of 5).

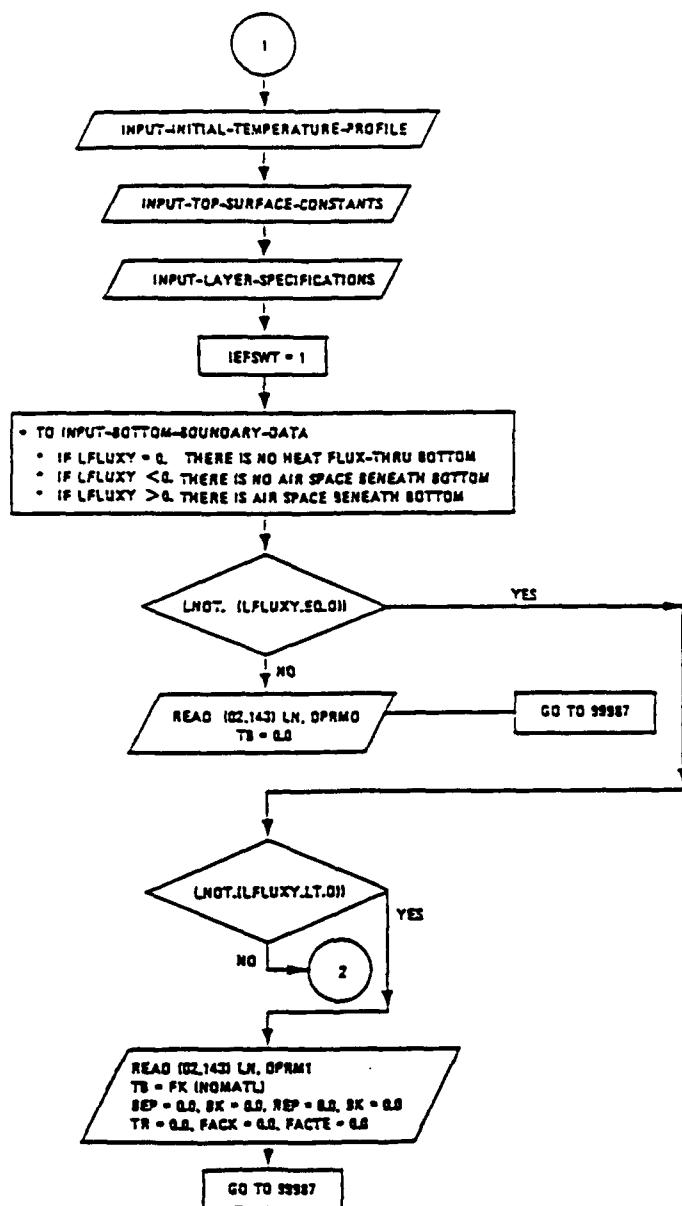


Figure 3.2. Simplified flowchart for TSTM, Balick et.al., 1981a  
(sheet 2 of 5).

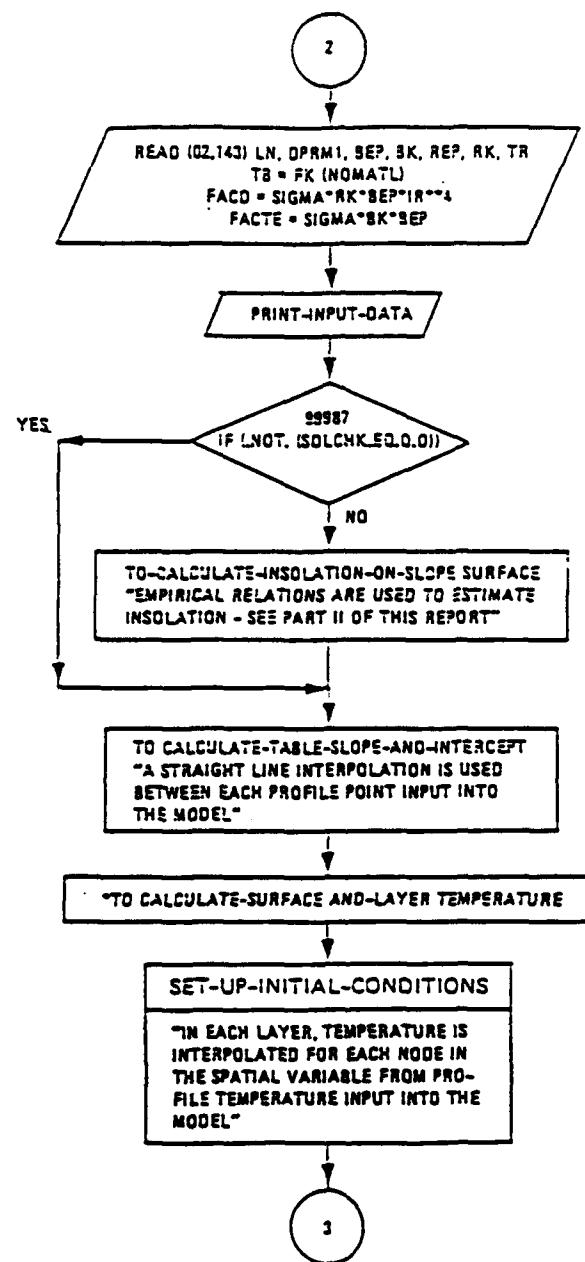


Figure 3.2. Simplified flowchart for TSTM, Balick *et.al.*, 1981a  
(sheet 3 of 5).

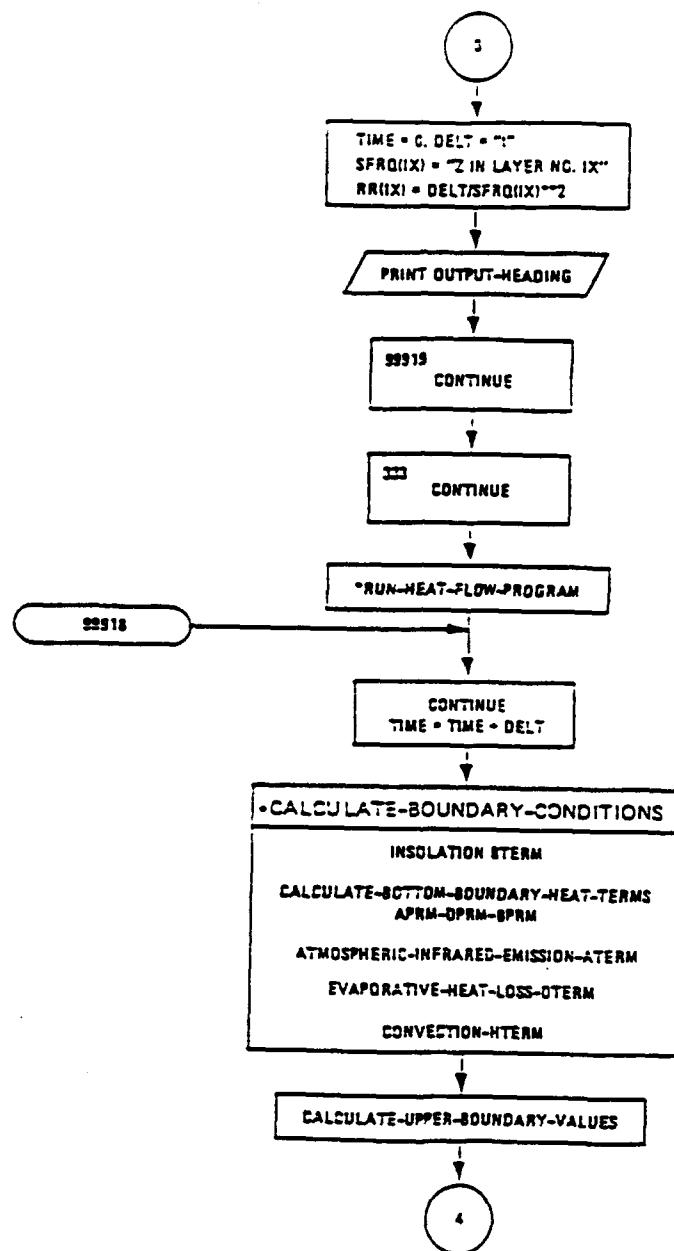


Figure 3.2. Simplified flowchart for TSTM, Balick et al., 1981a  
(sheet 4 of 5).

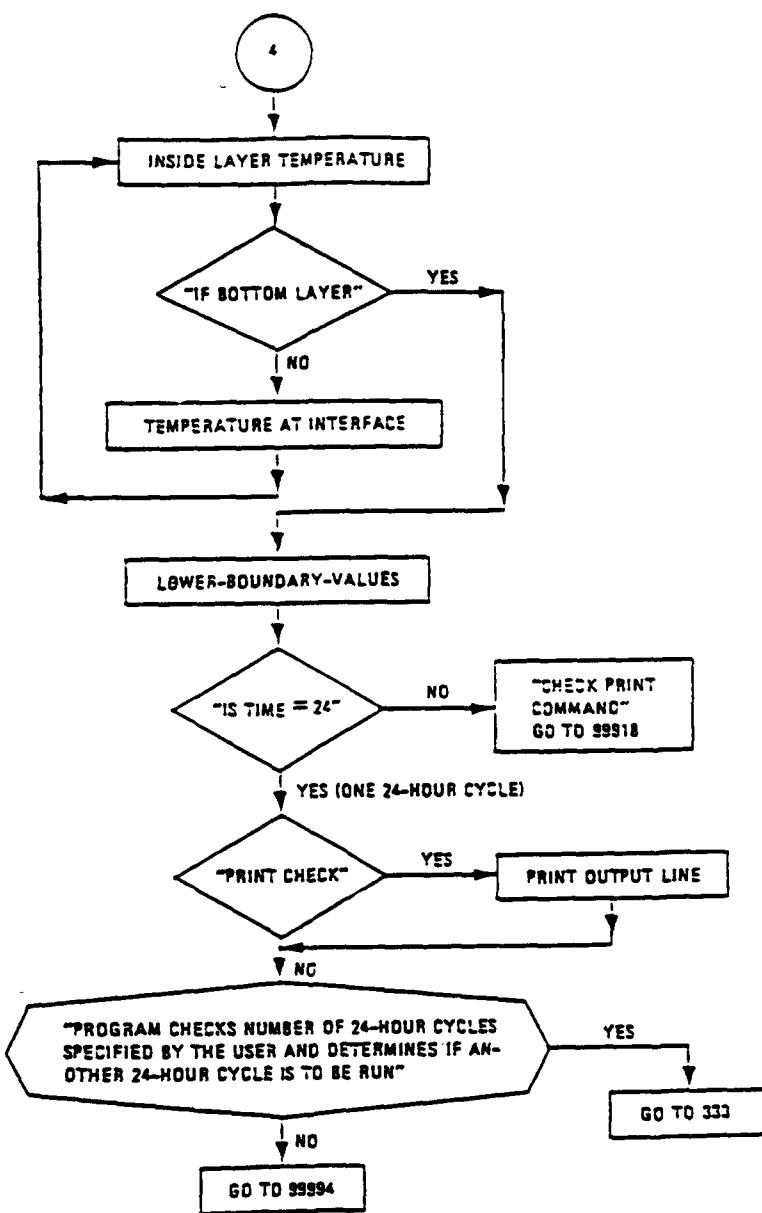


Figure 3.2. Simplified flowchart for TSTM, Balick *et.al.*, 1981a  
(sheet 5 of 5).

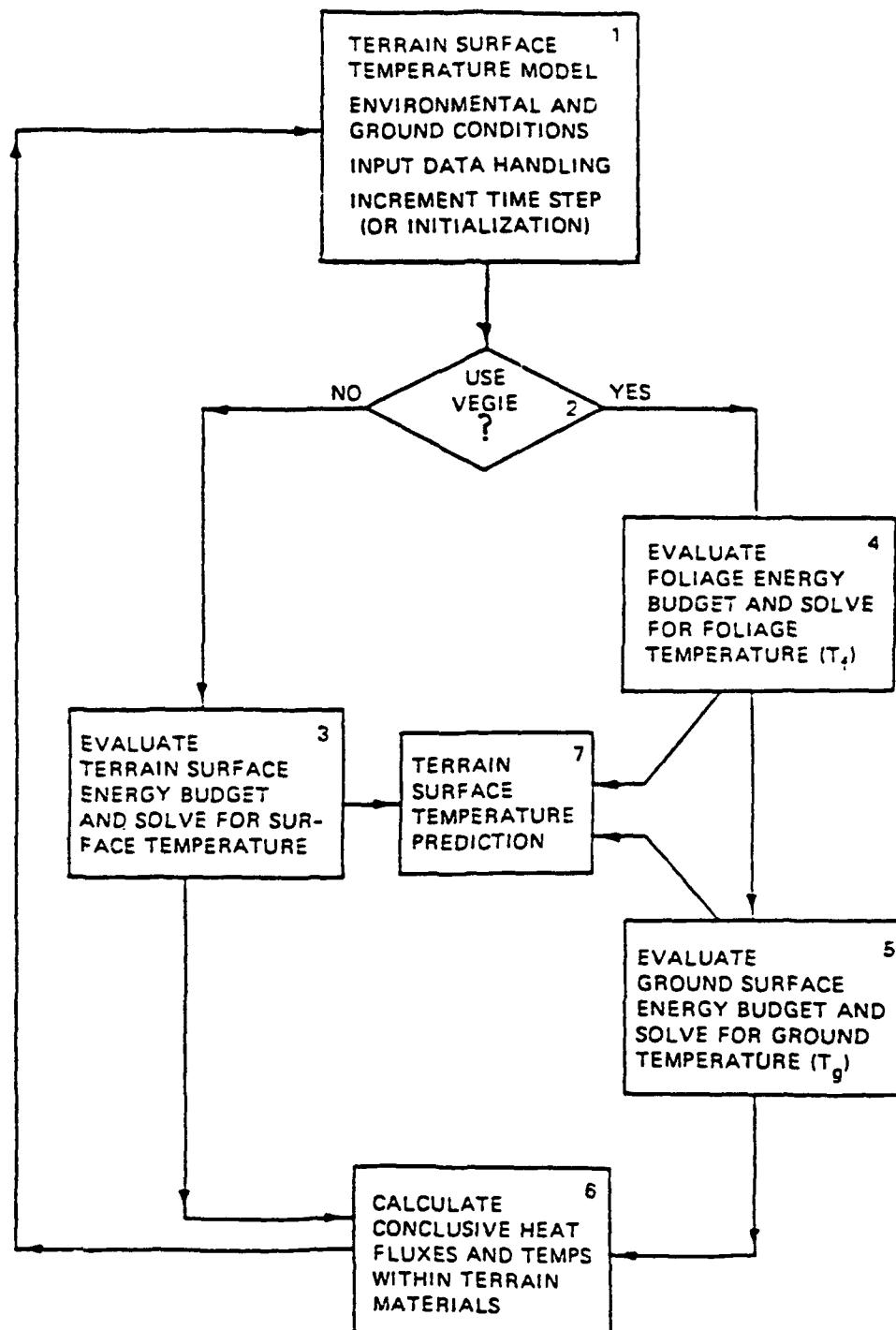


Figure 3.3. Sequence of calculation of the major components of the TSTM/VEGIE system, Balick et al. (1981b).

In block 1 the model is incremented one time step or initialized, or terminated) in accordance with procedures established for TSTM. In block 2 the decision whether to utilize VEGIE or not is made. If VEGIE is not used a non-vegetated surface energy budget is evaluated as an upper boundary condition (block 3) for the solution of the equation of heat transfer through the terrain materials (block 6). The solution for the surface temperature (block 7) comes from the evaluation of the surface energy budget equation and therefore to solve the heat transfer equation. In order to achieve this the heat conduction term and the distribution of heat in terrain materials must be calculated (block 6). If VEGIE is used, the energy budget of block 3 is replaced by blocks 4 and 5. Blocks 4 and 5 comprise VEGIE. Block 4 calculates the energy budget for the foliage that includes a contribution from the ground surface. Block 5 calculates the energy budget for the ground surface that includes a contribution from the foliage layer.

Solutions of temperature for the foliage (from block 4) and the ground (from block 5) are performed by a simple root-finding algorithm and are combined according to the proportion of foliage cover to yield an average, or effective, temperature of the vegetated surface. The ground energy budget is then used in the evaluation of heat flow in the terrain (block 6), and the programme returns to block 1.

### 3.2. Additional information.

SNOMO can be altered very simply in order to produce, in the output file, the hourly energy budget values for the snowpack of  $K_t$ ,  $K_f$ ,  $L_t$ ,  $L_f$ ,  $Q_c$  and  $Q_e$ . The alterations are found under the heading 'OPTION 2' in the hardcopy of the programme (section 3.3.)

The absence of a mass conservation routine was discussed in volume 1. A mass conservation routine has been written and tested (chapter 7, volume 1) and is included in the hardcopy of the

programme (section 3.3.) as 'OPTION 3'.

### 3.3. Programme code.

Copies of *snomo.f*, *snomo.dat*, *decid.dat*, *conif.dat*, *mix.dat*, *lapse.dat* and *SNOMO.RES* are available on the floppy disc inserted at the back of this volume. A fully commented hardcopy of the programme code is presented in the following pages.

C-----  
C SNOMO.F, JUNE 1991  
C BY  
C KATHERINE M. SAMBLES  
C-----

C  
C THIS IS A DISTRIBUTED PHYSICALLY-BASED SNOWMELT MODEL. SNOMO.F IS  
C DESIGNED TO OPERATE IN CONJUNCTION WITH A GIS DECISION AND DATA  
C MANIPULATION STRUCTURE WHICH DIVIDES THE CATCHMENT THAT IS TO BE  
C MODELLED INTO HOMOGENEOUS SUBDIVISIONS, CALLED CELLS. SNOMO.F  
C CALCULATES THE ENERGY-BUDGET OF THE SNOWPACK AT THE MID-POINT OF  
C ONE CELL AND CALCULATES THE RESULTANT CHANGE IN SNOWPACK PROPERTIES  
C AND MELTWATER RUNOFF. USING THE RESULTS FOR EACH CELL AND THE GIS  
C STRUCTURE A MAP OF THE SNOWCOVER DISTRIBUTION AND DEPTH DISTRIBUTION  
C CAN BE OBTAINED. SNOMO.F IS DEVELOPED FROM THE WES MODEL TSTM AND  
C THE SUBMODEL VEGIE WAS INCORPORATED INTO SNOMO.F IN MARCH 1989 WITH  
C THE HELP OF DR. RANDY SCOGGINS, WES.

C  
C SNOMO.F IS DIVIDED INTO 2 MAJOR PARTS:  
C (1) THE MAIN PROGRAM. THIS CALCULATES MELT, MANIPULATES THE  
C SNOWPACK DEPTH AND PHYSICAL CHARACTERISTICS AND HANDLES THE  
C MODEL INPUT AND OUTPUT.  
C (2) THE SUBROUTINE TSTM. THIS CALCULATES THE COMPONENTS OF THE  
C ENERGY-BUDGET OF THE SNOWPACK.

C SNOMO.F REQUIRES THE DATA FILES SNOMO.DAT, LAPSE.DAT, DECID.DAT,  
C MIX.DAT AND COMIF.DAT IN ORDER TO OPERATE. THE OUTPUT FILE IS  
C SNOMO.RES. A FULL LISTING OF ALL THE VARIABLES USED IS INCLUDED  
C AT THE END OF THE PROGRAM CODE.

C THERE ARE 3 CODE OPTIONS FOR SNOMO.F:  
C OPTION 1 IS THE DEFAULT OPTION. OPTION 1 IS UTILISED UNLESS OTHERWISE STATED.  
C OPTION 2 GIVES AN OUTPUT OF HOURLY ENERGY-BUDGET VALUES.  
C OPTION 3 INCLUDES A MASS CONSERVATION ROUTINE.

C  
C-----  
C

C INITIALISATION, DECLARATION, DATA STATEMENTS.

```
COMMON/MATRIX1/XXX(30,10),YYY(30,10)
COMMON/MATRIX2/DEPMX1(2,2),DEPMX2(3,2)
COMMON/MATRIX3/THICK1(1,6),THICK2(2,6)
COMMON/VECTOR/VNEWSN(1,6),VOLDSN(1,6)
COMMON/TSTM1/PRESS,NCLOUD,ZA,SLOPE1,SURFC1,DAY,LAT
COMMON/TSTM2/NOMATL,NIPTS
COMMON/VEGI/IVEG,SIGF,STATE,EFF,ALBEDO,HPOL
COMMON/RAIN/AIRTP
COMMON/SFRQ/SFRQ(6)
REAL SNPPW,SNVOL,CRITDP,NCAPSN,DENSN,
& DENV,NCAPW,LHTRATP,DEPTH,PTERM,NETRAD,AUSTP,
& AVETTP,PPTW,DAY1,LAT,TGRN,TSOL,TABSON,TAYTERM,TTERM,
& TDTERM,VSOIL(1,6),WE1,DEPTH1,MRSN,MRSN,BOTTP,STP,XSWTP,
& SPET1,SPHTW,SMDFP1,TMAX,TMIN
```

```

INTEGER I,J,N,K1,K2,K3,K10,K30,KONTRL,ILAPSE,IVEG,ISNOW,
& IRAIN,CELL,YEAR
C
C LATENT HEAT OF FUSION IS 0.334 MJkg-1
C SPECIFIC HEAT OF ICE IS GIVEN IN MJkg-1.K-1 = 2.10E+3 Jkg-1.K-1
C SPECIFIC HEAT OF WATER IS GIVEN IN KJkg-1.K-1 = 4.18E+3 Jkg-1.K-1
C
DATA DENW,HCAPW,HCAPSW,LHEATP/1000.0,4.21,2.09,0.334/
DATA SPETI,SPETIW/0.0021,4.18/
DATA TOTTIM,TPRQ,TPRNT/1.1.0,60.0/
NIN=10
NCONIF=11
NLAPSE=12
NDECID=13
NMIX=14
NOUT=9
OPEN(UNIT=NIN,FILE='SNOMO.DAT',STATUS='OLD')
REWIND NIN
OPEN(UNIT=NCONIF,FILE='CONIF.DAT',STATUS='OLD')
REWIND NCONIF
OPEN(UNIT=NLAPSE,FILE='LAPSE.DAT',STATUS='OLD')
REWIND NLAPSE
OPEN(UNIT=NDECID,FILE='DECID.DAT',STATUS='OLD')
REWIND NDECID
OPEN(UNIT=NMIX,FILE='MIX.DAT',STATUS='OLD')
REWIND NMIX
OPEN(UNIT=NOUT,FILE='SNOMO.RES')
REWIND NOUT
C
READ(10,*)CELL,YEAR
C
C VECTORS VNEMSN, VOLDSN AND VSOIL CONTAIN THE PHYSICAL
C PROPERTIES OF NEW SNOW, OLD SNOW AND SOIL RESPECTIVELY.
C VECTOR(1,1)= 0.0
C VECTOR(1,2)= SNOW/SOIL THERMAL DIFFUSIVITY, cm2min-1
C VECTOR(1,3)= SNOW/SOIL HEAT CONDUCTIVITY, calcm-2min-1.K-1
C VECTOR(1,4)= SNOW/SOIL EMISSIVITY, DECIMAL
C VECTOR(1,5)= SNOW/SOIL ALBEDO, DECIMAL
C VECTOR(1,6)= SNOW/SOIL DENSITY, gcm-3
C
READ(10,*)((VNEMSN(I,J),J=1,6),I=1,1)
READ(10,*)((VOLDSN(I,J),J=1,6),I=1,1)
READ(10,*)((VSOIL(I,J),J=1,6),I=1,1)
READ(10,*)PRESS,NLOUD,ZA
READ(10,*)SLOPE1,SURFC1,DAY1,LAT
READ(10,*)ILAPSE
READ(10,*)IVEG
READ(10,*)SNDP1
C
C IVEG DETERMINES WHICH VEGETATION DATA FILE IS USED:
C IVEG=1, CONIF.DAT (CONIFEROUS DATA)
C IVEG=2, DECID.DAT (DECIDUOUS DATA)

```

```

C IVEG=3, MIX.DAT (MIXED DATA)
C IVEG=0, NO VEGETATION DATA FILE IS USED, THE VEGETATION IS
C MODELLED AS PASTURE (OPEN) AND CLEARCUT.
C ILAPSE DETERMINES WHICH ELEVATION DATA FILE IS USED TO
C MODIFY THE AIR TEMPERATURES WITH LAPSE RATE. THE PRESENT
C USE OF ILAPSE REFERS SOLELY TO THE APPLICATION OF SNOMO.F TO
C THE W3 CATCHMENT.
C ILAPSE=0, ELEVATION BAND 1500-2000FT. THIS IS THE ELEVATION
C BAND OF THE METEOROLOGICAL STATION THAT PROVIDES THE INPUT
C DATA, THEREFORE NO CHANGES ARE MADE TO THE AIR TEMPERATURES.
C ILAPSE=1, ELEVATION BAND 1000-1500FT. THIS INCREASES THE
C MAX. AIR TEMP. BY 2°F AND THE MIN. BY 1°F.
C
      IF(IVEG.EQ.1)THEN
        READ(11,*)SIGF,STATE,EFF,ALBEDO,HFOL
      ELSE
        IF(IVEG.EQ.2)THEN
          READ(13,*)SIGF,STATE,EFF,ALBEDO,HFOL
        ELSE
          IF(IVEG.EQ.3)THEN
            READ(14,*)SIGF,STATE,EFF,ALBEDO,HFOL
          END IF
        END IF
      END IF
      IF(ILAPSE.GT.0)THEN
        READ(12,*)TMAX,TMIN
      END IF
      READ(10,*)CRITDP
      READ(10,*)SOILDP,SOILTP,SSOLTP
      READ(10,*)N
C
C N= NUMBER OF DAYS TO BE MODELLED IE. NO. OF DAYS IN DATA FILE
C MINUS ONE.
C DAILY METEOROLOGICAL DATA.
C XXX(1,8)= JULIAN DATE
C XXX(1,1)= OBSERVATION TIME, 24HR CLOCK
C YYY(1,1)= MINIMUM AIR TEMPERATURE, °C
C YYY(1,9)= MAXIMUM AIR TEMPERATURE, °C
C YYY(1,2)= RELATIVE HUMIDITY, %
C YYY(1,3)= CLOUD COVER, 0-1
C YYY(1,6)= WIND SPEED, m/s
C YYY(1,7)= PRECIPITATION, mm WATER
C
      READ(10,*)XXX(1,8),XXX(1,1),YYY(1,1),YYY(1,9),YYY(1,2),
      & YYY(1,3),YYY(1,6),YYY(1,7)
      READ(10,*)XXX(2,8),XXX(2,1),YYY(2,1),YYY(2,9),YYY(2,2),
      & YYY(2,3),YYY(2,6),YYY(2,7)
C
C SIMPLE MODIFICATION OF AIR TEMPERATURES FOR LAPSE RATE
      IF(ILAPSE.EQ.0)THEN
        GOTO 5
      ELSE

```

```

C CONVERT °C TO °F
YYY(1,1)=((YYY(1,1)*9.0)/5.0)+32.0
YYY(1,9)=((YYY(1,9)*9.0)/5.0)+32.0
YYY(2,1)=((YYY(2,1)*9.0)/5.0)+32.0
YYY(2,9)=((YYY(2,9)*9.0)/5.0)+32.0
IF(ILAPSE.EQ.1)THEN
  YYY(1,1)=YYY(1,1)+TMIN
  YYY(1,9)=YYY(1,9)+TMAX
  YYY(2,1)=YYY(2,1)+TMIN
  YYY(2,9)=YYY(2,9)+TMAX
ELSE
  YYY(1,1)=YYY(1,1)-TMIN
  YYY(1,9)=YYY(1,9)-TMAX
  YYY(2,1)=YYY(2,1)-TMIN
  YYY(2,9)=YYY(2,9)-TMAX
END IF
C CONVERT °F TO °C
YYY(1,1)=((YYY(1,1)-32.0)/9.0)*5.0
YYY(1,9)=((YYY(1,9)-32.0)/9.0)*5.0
YYY(2,1)=((YYY(2,1)-32.0)/9.0)*5.0
YYY(2,9)=((YYY(2,9)-32.0)/9.0)*5.0
END IF
C
C THE SNOWDEPTH AND THE PHYSICAL PROPERTIES OF THE
C SNOWPACK ARE HELD IN THE MATRICES DEPMX1, DEPMX2
C (HOLDING THE SNOWDEPTH AND CORRESPONDING TEMPERATURE)
C AND THKMX1, THKMX2 (HOLDING THE THICKNESS OF THE LAYERS
C OF THE PACK AND THE CORRESPONDING PHYSICAL PROPERTIES,
C IE. VNEWSN OR VOLDSN). THE NUMBERS 1 AND 2 REFER TO
C EITHER A 1- OR 2-LAYERED PACK, FOR A 1-LAYERED PACK
C NOMATL=1 AND NIPTS=2, FOR A 2-LAYERED PACK NOMATL=2,
C NIPTS=3.
C SET 2-LAYER SNOW THICKNESS MATRIX TO ZERO
C SET 2-LAYER DEPTH MATRIX TO ZERO
C
5      DO 20 I=1,2
        DO 10 J=1,6
          THKMX2(I,J)=0.0
10      CONTINUE
20      CONTINUE
        DO 40 I=1,3
          DO 30 J=1,2
            DEPMX2(I,J)=0.0
30      CONTINUE
40      CONTINUE
C
C SET CONTROLS TO ZERO
C WRITE HEADER FOR RESULTS FILE
C
KONTRL=0
SNVOL=0.0
DEPTH=0.0

```

```

K1=0
K2=0
K25=0
WRITE(9,*)'CELL NO.:',CELL
WRITE(9,*)'YEAR:',YEAR
WRITE(9,*)'JULIAN     SNOWDEPTH      SNOWMELT      SNOWFALL
& DENSITY RAIN-ON-SNOW'
WRITE(9,*)' DATE      (CM)    (CM SNOW) (MM WATER) (CM)
& (G/MM**3) (1=YES, 0=NO)'

C
C DAILY CALCULATION LOOP
C
DO 5001 L=1,N
K1=K1+1
K30=0
KELVIN=YYY(1,1)+273.15
PPTN=YYY(1,7)
AIRTP=YYY(1,1)
DDATE=XXX(1,6)
TIME2=XXX(2,1)

C
C LOGIC STRUCTURE TO INITIALISE SNOWDEPTH
C
IF(K3.EQ.1)THEN
K2=0
GOTO 57
ELSE
IF(PPTN.GT.0.0.AND.AIRTP.LT.0.0)THEN
SNPPTN=(PPTN/VNEWSN(1,6))/10
END IF
END IF
IF(K1.EQ.1)THEN
K2=0
SNPPTN=SNDP1
END IF
DEPTH=SNPPTN+DEPTH
IF(DEPTH.GE.CRITDP)THEN
IF(DEPTH.GT.CRITDP)THEN
NOMATL=2
NIPTS=3
DEPMX2(1,1)=0.0
DEPMX2(1,2)=AIRTP
DEPMX2(2,1)=5.0
DEPMX2(2,2)=AIRTP
DEPMX2(3,1)=SNPPTN
DEPMX2(3,2)=SSOLTP
XSNTP=((DEPMX2(1,2)+DEPMX2(3,2))/2)+273.15
DO 53 J=1,6
THRMX2(1,J)=VNEWSN(1,J)
THRMX2(2,J)=VOLDSN(1,J)
DEPMX2(1,1)=5.0
CONTINUE
53

```

```

THMKM2(2,1)=SNPPTN-5.0
ELSE
  NOMATL=1
  NIPTS=2
  DEPMK1(1,1)=0.0
  DEPMK1(1,2)=AIRTP
  DEPMK1(2,1)=DEPTH
  DEPMK1(2,2)=SSOLTP
  XSNTP=((DEPMK1(1,2)+DEPMK1(2,2))/2)+273.15
DO 54 J=1,6
  THMKM1(1,J)=VNEWSN(1,J)
54    CONTINUE
      THMKM1(1,1)=DEPTH
      END IF
      ISNOW=ISNOW+1
      K25=0
      K3=1
      K2=1
      GOTO 57
      ELSE
        NOMATL=1
        NIPTS=2
        DO 56 J=1,6
          THMKM1(1,J)=VSOIL(1,J)
56        CONTINUE
          THMKM1(1,1)=SOILDP
          DEPMK1(1,1)=0.0
          DEPMK1(1,2)=AIRTP
          DEPMK1(2,1)=SOILDP
          DEPMK1(2,2)=SOILTP
          K3=0
          K2=0
          END IF
C
C CALL SUBROUTINE CSFRQ, TO CALCULATE SFRQ
C
57    CALL CSFRQ(I,N)
C
C SET DEPTH MATRICES AND VARIABLES TO ZERO
C
      IF(NOMATL.EQ.1)THEN
        DO 59 I=1,3
          DO 58 J=1,2
            DEPMK2(I,J)=0.0
58        CONTINUE
59        CONTINUE
        ELSE
          DO 61 I=1,2
            DO 60 J=1,2
              DEPMK1(I,J)=0.0
60        CONTINUE
61        CONTINUE

```

```

END IF
K10=0
AVSTP=0.0
STP=0.0
AVSOL=0.0
AVGRR=0.0
AVABSR=0.0
AVATER=0.0
AVHTER=0.0
AVDTER=0.0
AVBTP=0.0
BOTTP=0.0
C
C CALL SUBROUTINE TSTM, TO CALCULATE THE SHORTWAVE, LONGWAVE, LATENT
C HEAT AND SENSIBLE HEAT EXCHANGES AT THE SURFACE OF THE SNOWPACK AND
C HEAT TRANSPORT THROUGH THE PACK. IN SNOMO TSTM CAN MODEL THESE
C EXCHANGES FOR EITHER SNOW OR SOIL.
C
CALL TSTM(I,'Y','N',K10,AVSTP,AVSOL,AVGRR,AVABSR,AVATER,
& AVHTER,AVDTER,K2,AVBTP,TGRR,TSOL,TABSOR,
& TATERM,TTERM,TDETERM)
C
C PROGRAM CONTINUES IF SNOW WAS MODELLED BY TSTM, JUMPS TO THE NEXT DAY
C IF SOIL WAS MODELLED
C
IF(K3.EQ.0)THEN
GOTO 9000
ELSE
K3=1
END IF
C
C CALL SUBROUTINE CMELT, TO CALCULATE THE MELT RATE. THE ENERGY
C INTRODUCED TO THE PACK BY RAIN (PTERM) IS NOT INCLUDED AT THIS STAGE
C MELT RATE IS CALCULATED IN CM OF SNOW AND MM OF WATER EQUIVALENT.
C
PTERM=0.0
CALL CMELT(I,N,NETRAD,PTERM,TSOL,TGRR,TABSOR,
& TATERM,TTERM,TDETERM,PPTN,DENSN,MRENE,MRSN,GTERM,DENW,DEPTH,
& AVSTP,AVBTP,XSNTP,SPHTI,K30)
IRAIN=0
C
C CALL SUBROUTINE RAINMP, TO CALCULATE THE ENERGY INTRODUCED TO THE
C MELTING PACK BY RAIN, IF RAIN OCCURED. THE MELT RATE IS RECALCULATED.
C
IF(PPTN.GT.0.0.AND.AIRTP.GT.0.0)THEN
IF(MRENE.GT.0.0)THEN
IRAIN=1
CALL RAINMP(I,N,PPTN,PTERM,DENW,K30)
CALL CMELT(I,N,NETRAD,PTERM,TSOL,TGRR,TABSOR,
& TATERM,TTERM,TDETERM,PPTN,DENSN,MRENE,MRSN,GTERM,DENW,
& DEPTH,AVSTP,AVBTP,XSNTP,SPHTI,K30)
END IF

```

```

        END IF
C
C CALCULATION OF SNOWFALL IF NOT FIRST ITERATION OR SOIL MODELLED
C IN THE PREVIOUS ITERATION.
C
IF(AVSTP.GT.0.0)THEN
AVSTP=0.0
END IF
IF(K2.EQ.0)THEN
IF(PPTN.GT.0.0.AND.AIRTP.LT.0.0)THEN
SNPPTN=(PPTN/VNEWSN(1,6))/10
K25=0
ELSE
SNPPTN=0.0
K25=K25+1
END IF
END IF
C
C LOGIC STRUCTURE TO ALLOW FOR THE EFFECTS OF SNOWFALL
C
IF(K1.EQ.1)THEN
DEPMX2(1,2)=AVSTP
DEPMX2(3,2)=AVBTTP
DEPMX2(2,2)=((DEPMX2(2,1)/DEPTH)*(AVBTTP-AVSTP))+AVSTP
GOTO 3000
END IF
IF(SNPPTN.GT.0.0)THEN
IF(NOMATL.EQ.1)THEN
IF(THRMX1(1,2).EQ.VNEWSN(1,6))THEN
IF(ISNOW.GT.0)THEN
THRMX1(1,1)=THRMX1(1,1)+SNPPTN
DEPTH=DEPTH+SNPPTN
DEPMX1(2,1)=DEPTH
DEPMX1(1,2)=AVSTP
DEPMX1(2,2)=AVBTTP
GOTO 4000
ELSE
WE1=(THRMX1(1,1)*10)*VNEWSN(1,6)
DEPTH1=(WE1/VOLDSN(1,6))/10
NOMATL=2
NIPTS=3
DO 70 J=1,6
THRMX2(1,J)=VNEWSN(1,J)
THRMX2(2,J)=VOLDSN(1,J)
CONTINUE
THRMX2(1,1)=SNPPTN
THRMX2(2,1)=DEPTH1
DEPTH=SNPPTN+DEPTH1
DEPMX2(1,2)=AVSTP
DEPMX2(3,2)=AVBTTP
DEPMX2(3,1)=DEPTH
DEPMX2(2,1)=THRMX2(1,1)
70

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DEPMX2(2,2)=((DEPMX2(2,1)/DEPTH)*(AVBTTP-AVSTP))+AVSTP
GOTO 3000
END IF
ELSE
NOMATL=2
NIPTS=3
DO 80 J=1,6
THKMX2(1,J)=VNEWSN(1,J)
THKMX2(2,J)=VOLDSN(1,J)
CONTINUE
THKMX2(1,1)=SNPPTN
THKMX2(2,1)=DEPTH
DEPTH=DEPTH+SNPPTN
DEPMX2(1,2)=AVSTP
DEPMX2(3,2)=AVBTTP
DEPMX2(3,1)=DEPTH
DEPMX2(2,1)=THKMX2(1,1)
DEPMX2(2,2)=((DEPMX2(2,1)/DEPTH)*(AVBTTP-AVSTP))+AVSTP
GOTO 3000
END IF
ELSE
IF(ISNOW.GT.0)THEN
THKMX2(1,1)=THKMX2(1,1)+SNPPTN
DEPTH=DEPTH+SNPPTN
DEPMX2(3,1)=DEPTH
DEPMX2(2,1)=THKMX2(1,1)
DEPMX2(2,2)=AVSTP
DEPMX2(3,2)=AVBTTP
DEPMX2(2,2)=((DEPMX2(2,1)/DEPTH)*(AVBTTP-AVSTP))+AVSTP
GOTO 3000
ELSE
WE1=(THKMX2(1,1)*10)*VNEWSN(1,6)
DEPTH1=(WE1/VOLDSN(1,6))/10
THKMX2(2,1)=THKMX2(2,1)+DEPTH1
THKMX2(1,1)=SNPPTN
DEPTH=THKMX2(2,1)+THKMX2(1,1)
DEPMX2(3,1)=DEPTH
DEPMX2(2,1)=THKMX2(1,1)
DEPMX2(1,2)=AVSTP
DEPMX2(3,2)=AVBTTP
DEPMX2(2,2)=((DEPMX2(2,1)/DEPTH)*(AVBTTP-AVSTP))+AVSTP
GOTO 3000
END IF
END IF
ELSE
IF(NOMATL.EQ.1)THEN
IF(THKMX1(1,2).EQ.VNEWSN(1,6))THEN
IF(ISNOW.GE.1)THEN
DEPMX1(1,2)=AVSTP
DEPMX1(2,2)=AVBTTP
GOTO 4000
ELSE

```

```

WE1=(THMK1(1,1)*10)*VNEWSN(1,6)
DEPTH1=(WE1/VOLDSN(1,6))/10
DEPTH=DEPTH1
DO 250 J=1,6
    THMK1(1,J)=VOLDSN(1,J)
CONTINUE
250
    THMK1(1,1)=DEPTH
    DEPMK1(1,2)=AVSTP
    DEPMK1(2,2)=AVBTTP
    DEPMK1(2,1)=DEPTH
    GOTO 4000
    END IF
    ELSE
        DEPMK1(1,2)=AVSTP
        DEPMK1(2,2)=AVBTTP
        GOTO 4000
        END IF
    ELSE
        IF(ISNOW.GT.0)THEN
            DEPMK2(1,2)=AVSTP
            DEPMK2(3,2)=AVBTTP
            DEPMK2(2,2)=((DEPMK2(2,1)/DEPTH)*(AVBTTP-AVSTP))+AVSTP
            GOTO 3000
        ELSE
            WE1=(THMK2(1,1)*10)*VNEWSN(1,6)
            DEPTH1=(WE1/VOLDSN(1,6))/10
            DEPTH=DEPTH1+THMK2(2,1)
            NOMATL=1
            NIPTS=2
            DO 350 J=1,6
                THMK1(1,J)=VOLDSN(1,J)
350
                CONTINUE
                THMK1(1,1)=DEPTH
                DEPMK1(1,2)=AVSTP
                DEPMK1(2,2)=AVBTTP
                DEPMK1(2,1)=DEPTH
                GOTO 4000
                END IF
            END IF
        END IF
C
C LOGIC STRUCTURE TO ALLOW FOR THE EFFECTS OF SNOWMELT
C ON A 2-LAYER PACK.
C
3000    IF(DEPTH.LE.5.0)THEN
        GOTO 5002
        END IF
C*****C*****C*****C*****C*****C*****C*****C*****C*****C*****C*****
C OPTION 3-MASS CONSERVATION ROUTINE.
C IF OPTION 3 REQUIRED INSERT MASS CONSERVATION ROUTINE TO REPLACE
C ALL CODE BETWEEN THE *****LINES.
C

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```

3001    IF(MRSN.GE.DEPTH)THEN
        GOTO 5002
    ELSE
        IF(MRSN.LE.0.0)THEN
            DEPMX2(1,2)=AVSTP
            DEPMX2(3,2)=AVBTP
            DEPMX2(3,1)=DEPTH
            DEPMX2(2,1)=THPMX2(1,1)
            DEPMX2(2,2)=((DEPMX2(2,1)/DEPTH)*(AVBTP-AVSTP))+AVSTP
            THPMX2(2,1)=DEPTH-THPMX2(1,1)
            GOTO 3500
        ELSE
            IF(MRSN.GE.THPMX2(1,1))THEN
                NOMATL=1
                NIPTS=2
                DO 400 J=1,8
                    THPMX1(1,J)=VOLDSN(1,J)
        400      CONTINUE
                DEPTH=DEPTH-MRSN
                THPMX1(1,1)=DEPTH
                DEPMX1(1,2)=AVSTP
                DEPMX1(2,2)=AVBTP
                DEPMX1(2,1)=THPMX1(1,1)
                ELSE
                    THPMX2(1,1)=THPMX2(1,1)-MRSN
                    DEPTH=THPMX2(1,1)+THPMX2(2,1)
                    DEPMX2(1,2)=AVSTP
                    DEPMX2(3,2)=AVBTP
                    DEPMX2(3,1)=DEPTH
                    DEPMX2(2,1)=THPMX2(1,1)
                    DEPMX2(2,2)=((DEPMX2(2,1)/DEPTH)*(AVBTP-AVSTP))+AVSTP
                    END IF
            3500      GOTO 5000
            END IF
        END IF
    C
    C LOGIC STRUCTURE TO ALLOW FOR THE EFFECTS OF SNOWMELT
    C ON A 1-LAYER PACK.
    C
4000    IF(DEPTH.LE.5.0)THEN
        GOTO 5002
    END IF
4001    IF(MRSN.GE.DEPTH)THEN
        GOTO 5002
    ELSE
        IF(MRSN.LE.0.0)THEN
            DEPMX1(1,2)=AVSTP
            DEPMX1(2,2)=AVBTP
            DEPMX1(2,1)=THPMX1(1,1)
            ELSE
                DEPTH=DEPTH-MRSN
                THPMX1(1,1)=DEPTH

```

```

DEPMX1(1,2)=AVSTP
DEPMX1(2,2)=AVBTP
DEPMX1(2,1)=THKMX1(1,1)
END IF
END IF

C
C IF TOP LAYER OF 2-LAYER PACK IS <1CM THICK THEN PACK IS
C CONVERTED INTO 1-LAYER PACK.
C
5000 IF(NOMATL.EQ.2.AND.THKMX2(1,1).LT.1.0)THEN
DEPTH=THKMX2(1,1)+THKMX2(2,1)
NOMATL=1
NIPTS=2
DO 450 J=1,6
THKMX1(1,J)=VOLDSW(1,J)
450 CONTINUE
THKMX1(1,1)=DEPTH
DEPMX1(2,1)=DEPTH
DEPMX1(1,2)=AVSTP
DEPMX1(2,2)=AVBTP
END IF

C
C MELTRATE CANNOT BE NEGATIVE.
C
IF(MRSN.LT.0.0)THEN
MRSN=0.0
END IF
IF(MRNE.LT.0.0)THEN
MRNE=0.0
END IF
550 FORMAT(6F6.2)
555 FORMAT(2F6.2)
*****
C END OF OPTION 3 CODE INSERTION.
C
C
C READ IN NEXT DAILY DATA LINE, SHIFTING EXISTING BOTTOM
C DATA LINE TO THE TOP. EXIT PROGRAM IF LAST DATA LINE
C REACHED.
C
9000 YYY(2,6)=YYY(2,6)/100.0
YYY(2,2)=YYY(2,2)*100
XXX(1,6)=XXX(2,6)
XXX(1,1)=TIME2
YYY(1,1)=YYY(2,1)
YYY(1,2)=YYY(2,2)
YYY(1,8)=YYY(2,9)
YYY(1,3)=YYY(2,3)
YYY(1,6)=YYY(2,6)
YYY(1,7)=YYY(2,7)
XXX(2,6)=0
XXX(2,1)=0

```

```

YYY(2,1)=0
YYY(2,8)=0
YYY(2,2)=0
YYY(2,3)=0
YYY(2,6)=0
YYY(2,7)=0
KONT=N-KONTRL
IF(NKONT.EQ.1)THEN
GOTO 5002
END IF
YYY(1,1)=YYY(1,1)-273.15
YYY(1,8)=YYY(1,8)-273.15
READ(10,* )XXX(2,8),XXX(2,1),YYY(2,1),YYY(2,8),YYY(2,2),
& YYY(2,3),YYY(2,6),YYY(2,7)
C
C CONVERT AIR TEMPERATURE FOR LAPSE RATE
C
IF(ILAPSE.EQ.0)THEN
GOTO 90
ELSE
C CONVERT °C TO °F
YYY(2,1)=((YYY(2,1)*9.0)/5.0)+32.0
YYY(2,8)=((YYY(2,8)*9.0)/5.0)+32.0
IF(ILAPSE.EQ.1)THEN
YYY(2,1)=YYY(2,1)+TMIN
YYY(2,8)=YYY(2,8)+TMAX
ELSE
YYY(2,1)=YYY(2,1)-TMIN
YYY(2,8)=YYY(2,8)-TMAX
END IF
C CONVERT °F TO °C
YYY(2,1)=((YYY(2,1)-32.0)/9.0)*5.0
YYY(2,8)=((YYY(2,8)-32.0)/9.0)*5.0
END IF
C
C REINITIALISATION OF CERTAIN VARIABLES, WRITE OUT RESULTS.
C
90 IF(K2.EQ.0)THEN
IF(SNPPTN.GT.0.0)THEN
ISNOW=ISNOW+1
ELSE
ISNOW=0
END IF
END IF
AIRT=YYY(1,1)
KELVIN=YYY(1,1)+273.15
PPTN=YYY(1,7)
DDATE=XXX(1,8)
KONTRL=KONTRL+1
SNOW=SNPPTN
SNPPTN=0.0
WRITE(8,333)DDATE-1,DEPTH,MRSW,MROWE,SNOW,DENSW,IRAIN

```

```
333  FORMAT(F6.2,5X,F6.2,4X,F6.2,4X,F6.2,4X,F6.2,7X,F6.2,5X,I3)
5001  CONTINUE
5002  WRITE(9,*)"PROGRAM TERMINATION"
      STOP
      END
C
C -----
```

```

C
C SUBROUTINE CMELT
C -----
C THIS CALCULATES THE MELTRATE IN CM OF SNOW AND MM OF WATER EQUIVALENT.
C THE DENSITY OF THE SNOWPACK IS CALCULATED IF THE PACK IS A 2-LAYERED
C PACK. MELT IS CALCULATED USING THE SNOW ENERGY-BUDGET. MOST OF
C THE COMPONENTS OF THE SNOW ENERGY-BUDGET ARE CALCULATED BY TSTM, THE
C EXCEPTIONS ARE PTERM AND DELQS. THE ENERGY UNITS ARE MJm-2day-1.
C
C
      SUBROUTINE CMELT(I,N,NETRAD,PTERM,TSOL,TGRB,TABSOR,
      & TATERM,TTERM,TDTERM,PPTN,DENSN,MREWE,MRSN,GTERM,DENW,DEPTH,
      & AVSTP,AVBTP,XSNTP,SPHTI,K30)
      COMMON/MATRIX2/DEPMX1(2,2),DEPMX2(3,2)
      COMMON/MATRIX3/THRMX1(1,6),THRMX2(2,6)
      COMMON/TSTM2/NOMATL,NIPTS
      REAL LHEATF,NETRAD,MREWE,MRSN,DEPTH,DENSN,A,B,C,D,
      & XSNTP1,DELQS,DELREWE,DELSRN,XSNTP
      DATA LHEATF,BCAPW,BCAPSN/0.334,4.21,2.09/
      GTERM=0.0
C
C CALCULATION OF THE DENSITY OF SNOW
C
      IF(NOMATL.EQ.1)THEN
      DENSN=THRMX1(1,6)
      ELSE
      A=THRMX2(1,1)/DEPTH
      B=THRMX2(2,1)/DEPTH
      C=A*THRMX2(1,6)
      D=B*THRMX2(2,6)
      DENSN=C+D
      END IF
C
C CALCULATION OF DELQS IN Jm-2day-1, THEN CONVERTED TO MJm-2dy-1
C
      IF(K30.EQ.1)THEN
      K30=0
      GOTO 10
      ELSE
      XSNTP1=XSNTP
      XSNTP=((AVSTP+AVBTP)/2)+273.15
      DELQS=((DEPTH*0.01)*(DENSN*1000))*((SPHTI*XSNTP)-
      & (SPHTI*XSNTP1))
      END IF
C
C CALCULATION OF THE ENERGY-BUDGET OF THE SNOWPACK AND THE MELT RATE.
C MULTIPLY MREWE BY 1000, SO THAT RESULT IS IN MM WATER.
C MULTIPLY MRSN BY 100, SO THAT RESULT IS IN CM SNOW.
C
      10   NETRAD=TSOL-(TSOL-TABSOR)+TATERM-TGRB
      DELQM=NETRAD+TDTERM+TTERM+GTERM+PTERM-DELQS
      DELREWE=(DELQM/(LHEATF*DENW))*1000
      DELRSN=(DELQM/(LHEATF*(DENSN*1000)))*100

```

MNAME=DELNAME

MRSN=DELRSN

RETURN

XEND

C

C -----

```
C
C SUBROUTINE RAINMP
C -----
C CALCULATES THE ENERGY INPUT TO THE PACK BY RAIN FALLING ON
C A MELTING PACK AT 0OC. THE EQUATION IS TAKEN FROM MALE &
C GRAY (1981). THE UNITS ARE MJm-2 dy-1.
C
SUBROUTINE RAINMP(I,N,PPTN,PTERM,DENW,K30)
COMMON/RAIN/AIRTP
REAL PTERM
DATA LHEATF,BCAPSN,BCAPW/0.334,2.09,4.21/
DATA SPHTW/4.18/
PTERF=(DENW*SPHTW*AIRTP*PPTN)/1000
PTERF=PTERM/1000
K30=1
RETURN
END
C
C -----
```

```
C SUBROUTINE CSFRQ
C -----
C CALCULATES SFRQ, THE VERTICAL GRID SPACING IN EACH
C COMPUTATIONAL LAYER.
C
SUBROUTINE CSFRQ(I,N)
COMMON/MATRIX3/THKMX1(1,6),THKMX2(2,6)
COMMON/VECTOR/VNEWSN(1,6),VOLDSN(1,6)
COMMON/TSTM2/NOMATL,NIPTS
COMMON/VEGI/IVEG,SIGF,STATE,EFF,FOLA,HFOL
COMMON/SFRQ/SFRQ(6)
REAL SFRQ1,SFRQ2
DATA TOTTIM,TFRQ,TPRNT/1,1.0,60.0/
C
C CALCULATION OF SFRQ FOR LAYER 1
C
IF(NOMATL.EQ.1)THEN
SFRQ1=(THKMX1(1,1))/2
ELSE
SFRQ1=(THKMX2(1,1))/2
END IF
100 IF(SFRQ1.LE.5.0)THEN
GOTO 200
ELSE
IF(SFRQ1.LE.10.0)THEN
GOTO 200
ELSE
SFRQ1=SFRQ1/2
GOTO 100
END IF
END IF
200 SFRQ(1)=SFRQ1
C
C CALCULATION OF SFRQ FOR LAYER 2, IF NECESSARY
C
IF(NOMATL.EQ.2)THEN
SFRQ2=THKMX2(2,1)/2
300 IF(SFRQ2.LE.5.0)THEN
GOTO 400
ELSE
IF(SFRQ2.LE.10.0)THEN
GOTO 400
ELSE
SFRQ2=SFRQ2/2
GOTO 300
END IF
END IF
400 SFRQ(2)=SFRQ2
END IF
C
C CALCULATION OF TIMESTEP ENSURING NUMERICAL STABILITY.
C
```

```
IF(NOMATL.EQ.1)THEN
TIMSP1=0.5*(SFRQ(1)*SFRQ(1)/VNEWSN(1,2))
ELSE
TIMSP1=0.5*(SFRQ(1)*SFRQ(1)/VNEWSN(1,2))
TIMSP2=0.5*(SFRQ(2)*SFRQ(2)/VOLDSN(1,2))
TIMSP1=MIN(TIMSP1,TIMSP2)
END IF
ITIME=INT(TIMSP1)
IF(ITIME.EQ.0)ITIME=1
IF(ITIME.GT.5)ITIME=5
IF(IVEG.EQ.1)ITIME=1
TFRQ=REAL(ITIME)
RETURN
END

C
C -----
```

```

C
C SUBROUTINE TSTM
C -----
C CALCULATES THE SHORTWAVE, LONGWAVE, LATENT HEAT AND SENSIBLE HEAT
C EXCHANGES OVER THE SNOWPACK OR SOIL SURFACE, AND THE HEAT TRANSPORT
C THROUGH THE SOIL OR SNOW. TSTM HAS BEEN CONVERTED INTO A SUBROUTINE
C FROM BALICK ET.AL. (1981a & b). THE CONVERSION OF TSTM AND INCLUSION
C OF VEGIE WAS AIDED BY DR. RANDY SCOGGINS (WES). VEGETATED SURFACES
C ARE MODELLED USING THE SUBMODEL VEGIE. TSTM WAS ORIGINALLY THE TERRAIN
C SURFACE TEMPERATURE MODEL AND ITS FUNCTION WAS TO PREDICT SURFACE
C TEMPERATURE.
C
C
C
      SUBROUTINE TSTM(I,AN1,AN,K10,AVSTP,AVGBR,AVSOL,AVABSR,
     & AVATER,AVHTER,AVDTER,K2,AVBTP,TGBR,TSOL,TABSOR,TATERM,
     & THTERM,TDTERM)
C
C INITIALISATION, DECLARATION AND DATA STATEMENTS
C
      INTEGER OUTCD
      DIMENSION DATMK(100,10)
      DIMENSION RHOC(6),MAX(10),DEPTH(450),FMM(30,10),BBB(30,10)
      DIMENSION TITLE(7)
      DIMENSION NK(6),ATF(2),FEB(2)
      DIMENSION RR(6),INTR(7)
      DIMENSION THK(6),ALPH(6),FK(6),STOR(7,450),STABN(6)
      REAL KTEMPG,KTEMPA,LAT,ACL(8),BCL(8),M,KSQ,BOTTP,WET,
     & ISOL,IGBR,IABSOR,IATERM,IHTERM,IDTERM,ISURFG,IREFRA,
     & SLOPE,SURFAC,CLR(8)
      CHARACTER HEADER*72,AN*1,AN1*1
      COMMON/MATRIX1/XCC(30,10),YYY(30,10)
      COMMON/MATRIX2/DEPMX1(2,2),DEPMX2(3,2)
      COMMON/MATRIX3/THKMX1(1,6),THKMX2(2,6)
      COMMON/TSTM1/PRESS,NCLOUD,ZA,SLOPE1,SURFC1,DAY,LAT
      COMMON/TSTM2/NOMATL,NIPTS
      COMMON/VEGI/IVEG,SIGF,STATE,EFF,ALBEDO,HFOL
      COMMON/SFRQ/SFRQ(6)
      DATA TOTTIM,TFRQ,TPRNT/1,1.0,60.0/
      DATA CLR/0.04,0.08,0.17,0.20,0.22,0.24,0.24,0.25/
      DATA OUTCD/0/
      DATA ACL/82.2,87.1,52.5,39.0,34.7,23.8,11.2,15.4/
      DATA BCL/.079,.148,.112,.063,.104,.159,-.167,.028/
      DATA SIGMA,PI,AC,BC/8.12E-11,3.141593,17.269,35.86/
      DATA CC/0.281/
      DATA LAST,G,KSQ,CP/2,980.0,0.16,0.24/
C
C STATEMENT FUNCTIONS FOR USE IN VEGETATION SECTION
C
      E(T)=8E+6.108*EXP(AC*(T-273.15)/(T-BC))
      EBAT(T)=6.108*EXP(AC*(T-273.15)/(T-BC))
      Q(T)=0.622/(PRESS/E(T)-.378)

```

```

QSAT(T)=0.622/(PRESS/ESAT(T)-.378)

C
C CONVERSION OF VARIABLES PASSED FROM MAIN PROGRAM INTO FORM
C USED IN TSTM. 1 OR 2-LAYERED SNOWPACK USED.
C

      IFLAG2=0
      IRETRN=0
      IPRNT=0
      SUM=0.0
      IF(NOMATL.EQ.1)THEN
        XXX(1,5)=DEPMX1(1,1)
        YYY(1,5)=DEPMX1(1,2)
        XXX(2,5)=DEPMX1(2,1)
        YYY(2,5)=DEPMX1(2,2)
        THK(1)=THKMX1(1,1)
        ALPH(1)=THKMX1(1,2)
        FK(1)=THKMX1(1,3)
        EPSN=THKMX1(1,4)
        SMALLA=(1-THKMX1(1,5))
      ELSE
        XXX(1,5)=DEPMX2(1,1)
        YYY(1,5)=DEPMX2(1,2)
        XXX(2,5)=DEPMX2(2,1)
        YYY(2,5)=DEPMX2(2,2)
        XXX(3,5)=DEPMX2(3,1)
        YYY(3,5)=DEPMX2(3,2)
        THK(1)=THKMX2(1,1)
        THK(2)=THKMX2(2,1)
        ALPH(1)=THKMX2(1,2)
        ALPH(2)=THKMX2(2,2)
        FK(1)=THKMX2(1,3)
        FK(2)=THKMX2(2,3)
        EPSN=THKMX2(1,4)
        SMALLA=(1-THKMX2(1,5))
      END IF
-----
C
C     INITIALIZE-VARIABLES-AND-CONSTANTS
99996  ASSIGN 99994 TO I99995
      GO TO 99995
99994  CONTINUE
-----
C
C     INPUT-DATA
      ASSIGN 99989 TO I99990
      GO TO 99990
-----
C
C     PRINT-INPUT-DATA
99989  ASSIGN 99987 TO I99988
      IF(AN1.EQ.'Y')GO TO 99988
99987  CONTINUE
-----
C
C     CALCULATE-TABLE-SLOPE-AND-INTERCEPT
99986  ASSIGN 99982 TO I99983

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```

GO TO 99983
C-----
C      CALCULATE-SURFACE-AND-LAYER-TEMPERATURE
99982  CONTINUE
      ASSIGN 99980 TO I99981
      GO TO 99981
C-----
99980  CONTINUE
      PPTN=(YYY(1,7)+YYY(2,7))/2
C
C CALCULATION OF DAILY TOTALS FOR THE ENERGY-BUDGET VARIABLES
C REQUIRED BY THE MAIN PROGRAM.
C
      SUMC2=0
      SUMC3=0
      SUMC4=0
      SUMC5=0
      SUMC6=0
      SUMC7=0
      SUMC8=0
      SUMC9=0
      DO 99 I=1,K10
      SUMC2=SUMC2+DATMX(I,2)
      SUMC3=SUMC3+DATMX(I,3)
      SUMC4=SUMC4+DATMX(I,4)
      SUMC5=SUMC5+DATMX(I,5)
      SUMC6=SUMC6+DATMX(I,6)
      SUMC7=SUMC7+DATMX(I,7)
      SUMC8=SUMC8+DATMX(I,8)
      SUMC9=SUMC9+DATMX(I,9)
99    CONTINUE
C
C CONVERT DAILY ENERGY TOTALS IN lyhr-1 TO MJm-2day-1
C
      TGBR=SUMC3/24
      TSOL=SUMC4/24
      TABSOR=SUMC5/24
      TATERM=SUMC6/24
      TTERM=SUMC7/24
      TDTERM=SUMC8/24
C
C CALCULATION OF MEAN DAILY ENERGY VALUES IN MJm-2
C AND MEAN SURFACE AND BASAL TEMPERATURES ('C).
C
      AVSTP=SUMC2/K10
      AVGBR=(SUMC3/K10)/24
      AVBOL=(SUMC4/K10)/24
      AVABSR=(SUMC5/K10)/24
      AVATER=(SUMC6/K10)/24
      AVTER=(SUMC7/K10)/24
      AVDTER=(SUMC8/K10)/24
      AVBTTP=SUMC9/K10

```

```

C
C RETURN TO MAIN PROGRAM
C
      WRITE(*,*)'NORMAL TERMINATION'
C-----
C      STOP
      RETURN
C-----
C-----99997 CONTINUE
C FORMATS
 90  FORMAT(' BOTTOM BOUNDARY INDEX=',I3)
 92  FORMAT(' BOTTOM BOUNDARY TEMPERATURE=',F6.1,' DEG C')
 95  FORMAT(' BOTTOM BOUNDARY HEAT FLUX=',F6.1,'W/M**2')
 97  FORMAT(F11.2,F11.1,F13.2,F13.1,F8.2)
120  FORMAT(A8,F8.1)
140  FORMAT(F5.1,F10.1,F6.1,F12.1,F12.1,F13.1)
145  FORMAT(F6.1,F7.1)
150  FORMAT(F12.1,I12,F11.2)
160  FORMAT(F11.2,F13.2,F8.1,F10.1)
170  FORMAT(F9.4,F12.1)
180  FORMAT(I7,F16.1,F11.0,F12.0)
C190  FORMAT(4X,F5.2,F6.1,2X,I8,I9,I11,I9,I9,I8)
190  FORMAT(4X,F5.2,F6.1,F6.2,F6.2,F6.2,F6.2,F6.2)
260  FORMAT(9X,F8.1,F11.2,F9.2,F9.2,F8.2,F10.2,F8.2)
200  FORMAT(F8.2,F8.2)
210  FORMAT(I6,F11.1,F12.1,F14.2,F14.2)
220  FORMAT(1H1)
230  FORMAT(A72)
240  FORMAT(4X,F7.2,2X,F5.0,5X,F6.2,10X,F6.2,9X,F7.2)
250  FORMAT(6X,F8.1,13X,F4.1,12X,F5.1)
310  FORMAT(11X,'TOTAL GRAYBODY EFFECTIVE GROUND FOLIAGE',
     &           4X,'SOLAR')
320  FORMAT(14X,'RADIANCE TEMP',10X,'TEMP TEMP'
     & ,4X,'INSOLATION')
330  FORMAT(5X,'HR',7X,'(LANGLEYS)',9X,'(C)',11X,'(C)'
     & ,6X,'(C) (LANGLEYS)')
340  FORMAT(9X,'----REFL-NREFL----REFL----NREFL',30(1H-))
270  FORMAT(3X,F5.2,F8.2,F8.2,2X,F8.2,F8.2,F8.2,F8.2,F8.2)
350  FORMAT(57X,'SENSIBLE LATENT')
360  FORMAT(5X,'HRS SURFACE GRAYBODY SOLAR SURFACE ATMOS',
     & ' IR HEAT HEAT')
370  FORMAT(11X,'TEMP RADIANCE INSOLATION ABSORP EMISSION',
     & ' LOSS FLUX')
380  FORMAT(11X,'DEG C',23(1H-),'(LANGLEYS)',24(1H-))
390  FORMAT(3X,'TIME',16X,'DEPTH, TEMPERATURE'/4X,'HR',21X,'CM',
     & 9X,'C'/2X,65(1H-))
400  FORMAT(2E0 ,F5.2,4(3X,F5.1,' ',F5.2))
410  FORMAT(10X,F5.1,1X,F5.2,3X,F5.1,1X,F5.2,3X,F5.1,1X,F5.2,
     & 3X,F5.1,1X,F5.2)
      GO TO I99997
C-----
```

```
99995 CONTINUE
C   TO INITIALIZE-VARIABLES-AND-CONSTANTS
    BB=-2.4E-4
    MAX(1)=2
    MAX(2)=2
    MAX(3)=2
    MAX(4)=2
    MAX(5)=NIPTS
    MAX(6)=2
    MAX(7)=2
    MAX(8)=0
    MAX(9)=0
    MAX(10)=3
    IBUG=0
    IEOF=0
    GO TO I99995
C-----
99990 CONTINUE
C   TO INPUT-DATA
C
C   INPUT-ATMOSPHERIC-SPECIFICATIONS
    ASSIGN 99978 TO I99979
    GO TO 99979
C
C   INPUT-SURFACE-ORIENTATION-SPECIFICATIONS
    99978 ASSIGN 99976 TO I99977
    GO TO 99977
C
C   INPUT-HEAT-FLOW-CACULATION-CONTROLS
    99976 ASSIGN 99974 TO I99975
    GO TO 99975
C
C   INPUT-INITIAL-TEMPERATURE-PROFILE
    99974 ASSIGN 99972 TO I99973
    GO TO 99973
C
C   INPUT-TOP-SURFACE-CONSTNTS
    99972 ASSIGN 99970 TO I99971
    GO TO 99971
C
C   INPUT-LAYER-SPECIFICATIONS
    99970 ASSIGN 99968 TO I99969
    GO TO 99969
C
C   INPUT-BOTTOM-BOUNDARY-DATA
    99968 ASSIGN 99966 TO I99967
    GO TO 99967
C
C   INPUT-VEGETATION-PARAMETERS
    99966 ASSIGN 99798 TO I99799
    GO TO 99799
C
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99798 GO TO I99990
C-----
99979 CONTINUE
C   TO INPUT-ATMOSPHERIC-SPECIFICATIONS
C
C   LINE    TIME    AIR TEMP RH  CLOUD COVER WIND SPEED, INSOLATION
C   NO.     HR      DEG C   I (0-1)      M/3      CAL/CM**2-MIN
C
C   XXX(2,1)=XXX(2,1)+2400*(XXX(2,8)-XXX(1,8))
860 DO 99985 J=1,2
  XXX=INT(XXX(J,1)/100.0)*100
  AXXX=(XXX(J,1) - REAL(XXX))/60.0
  XXX(J,1)=REAL(XXX)/100.0+AXXX
  XXX(J,7)=XXX(J,1)
  XXX(J,2)=XXX(J,1)
  XXX(J,3)=XXX(J,1)
  XXX(J,4)=XXX(J,1)
  XXX(J,6)=XXX(J,1)
  YYY(J,1)=YYY(J,1)+273.1
  YYY(J,9)=YYY(J,9)+273.15
  YYY(J,2)=YYY(J,2)*0.01
  YYY(J,6)=YYY(J,6)*100.0
  YYY(J,4)=YYY(J,4)/697.6
99985 CONTINUE
  XXX(3,10)=XXX(2,1)
  XXX(2,10)=14.0
  XXX(1,10)=XXX(1,1)
  YYY(3,10)=YYY(2,1)
  YYY(2,10)=YYY(1,9)
  YYY(1,10)=YYY(1,1)
C
840 FACTRH=(1000.0/PRESS)**0.286
GO TO I99979
C-----
99977 CONTINUE
C   TO INPUT-SURFACE-ORIENTATION-SPECIFICATIONS
C
C   LINE SPC SLOPE    SPC AZIMUTH   DAY      LATITUDE
C   NO.  DEG-BORIZ=0 DEG S=0      JULIAN  DEG
C
C   SLOPE=SLOPE1
C   SURFAC=SURFC1
C   SLOPE=SLOPE*PI/180.0
C   SURFAC=SURFAC*PI/180.
GO TO I99977
C-----
99975 CONTINUE
C   TO INPUT-HEAT-FLOW-CACULATION-CONTROLS
C
C   LINE NO. OF NO. OF 24 HRS TIME STEP PRINT FREQ
C   NO. LAYERS REPICTIONS      MIN      MIN
C           1-6      2-5

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```
C
      TOTTEM=XXX(2,1) - XXX(1,1)
      GO TO I99975
C-----
99973  CONTINUE
C     TO INPUT-INITIAL-TEMPERATURE-PROFILE
C
C     LINE NO. OF
C     NO. PROFILE POINTS
C
C
C     LINE DEPTH TEMP
C     NO. CM    DEG C
C
MAX(5)=NIPTS
DO 99964 J3=1,NIPTS
YYY(J3,5)=YYY(J3,5)+273.15
99964  CONTINUE
GO TO I99973
C-----
99971  CONTINUE
C     TO INPUT-TOP-SURFACE-CONSTANTS
C     LINE EMISSIVITY ABSORBTIVITY MOISTURE
C     NO.                 CONTENT DRY WT.
C
FACTA=SIGMA*EPSN
C
GO TO I99971
C-----
99967  CONTINUE
C     TO INPUT-BOTTOM-BOUNDARY-DATA
C
C     IF LFLUXY=0, THERE IS NO HEAT FLUX THROUGH BOTTOM
C     IF IFLUXY LT 0, THERE IS NO AIRSPACE BEHNEATH BOTTOM
C     IF IFLUXY GT 0, THERE IS AIRSPACE BEHNEATH BOTTOM
C
LFLUXY=-1
IF(.NOT.(LFLUXY.EQ.0)) GO TO 99962
DPRM0=YYY(NIPTS,5)
TB=0.
GO TO 99963
99962 IF(.NOT.(LFLUXY.LT.0)) GO TO 99961
C
DPRM1=-0.5
TB=PK(NOMATL)
REP=0.0
BK=0.
REF=0.
TR=0.0
FACTD=0.
FACTE=0.
RK=0.
```

```

DPRM1=DPRM1/697.6
GO TO 99963
99961 CONTINUE
99963 GO TO I99967
C-----
99969 CONTINUE
C   TO INPUT-LAYER-SPECIFICATIONS
C
C       LINE THICKNESS VERT. GRID THERMAL DIFF HEAT COND
C       NO. CM      SPACE-CM  CM**2/MIN  CAL/MIN-CM-K
C
C       DO 99960 J4=1,NOMATL
C          RBC(J4)=PK(J4)/ALPH(J4)
99960 CONTINUE
C   CONTROL SWITCHES SPECIFIED
C
C       NIT=1
C       IKFSWT=1
C       GO TO I99969
C-----
99799 CONTINUE
C   TO INPUT-VEGETATION-PARAMETERS
C   IVEG DETERMINES WHETHER VEGETATION PARAMETERS ARE USED
C   OR NOT. HEIGHT OF THE METEOROLOGICAL INSTRUMENTS FROM
C   WHICH THE DAILY DATA ARE TAKEN ARE ASSUMED TO BE 100CM
C   ABOVE THE FOLIAGE HEIGHT. SEE TEXT FOR FULLER EXPLANATION.
C
C       IF(IVEG.EQ.0) GO TO 1120
C       POLA=1-ALBEDO
C       IF(HPOL.GE.ZA)THEN
C          ZA=HPOL+100.0
C       END IF
C       IF(SIGF.LE.0.0)GO TO I99798
C       TF=YYY(1,1)
C       IVEG=1
C       EP1=EPP+EPSN-EPP*EPSN
C       Z0=0.131*HPOL**0.997
C       CH0=KSQ/( ALOG(ZA/Z0)**2)
C       ZDSP=0.701*HPOL**0.979
C       CRR=KSQ/( ALOG((ZA-ZDSP)/Z0)**2)
C       CHG=(1.-SIGF)*CH0+SIGF*CRR
C       DELIMP=1.
C       QAP=QSAT(TF)
1120  GO TO I99799
C-----
99988 CONTINUE
C   TO PRINT-INPUT-DATA
C   WRITE(*,139)
C   WRITE(*,220)
C   WRITE(*,' ')
C   WRITE(*,230)HEADER
C   WRITE(*,' ')

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      WRITE(*,*)' ATMOSPHERIC-SPECIFICATIONS'
      WRITE(*,*)'
      WRITE(*,*)' ATMOS PRESS CLOUD TYPE SHELTER'
      WRITE(*,*)' MS INDEX HEIGHT-CM'
      WRITE(*,150)PRESS,NCLOUD,ZA
      WRITE(*,*)'
      WRITE(*,*)' TIME AIR TEMP RH CLOUD COVER WIND SPEED'
&   , ' SOLAR IRRAD'
      WRITE(*,*)' HRS DEG C Z (0-1) M/S W/M**2'
      MMAX=2
      WRITE(*,140)(XXX(J,1),YYY(J,1)-273.15,
& YYY(J,2)*100.0,YYY(J,3),YYY(J,6)*0.01,YYY(J,4)*697.6,J=1,MMAX)
      WRITE(*,*)'
      WRITE(*,*)' SURFACE-ORIENTATION-SPECIFICATIONS'
      WRITE(*,*)'
      WRITE(*,*)' SPC SLOPE SPC AZIMUTH DAY LATITUDE'
      WRITE(*,*)' DEG-HORIZ=0 DEG S=0 JULIAN DEG'
      WRITE(*,180)SLOPE*180/PI,SURFAC*180.0/PI,DAY,LAT
      WRITE(*,220)
      WRITE(*,*)' HEAT-FLOW-CACULATION-CONTROLS'
      WRITE(*,*)'
      WRITE(*,*)' NO. OF NO. OF 24 HRS TIME STEP PRINT FREQ'
      WRITE(*,*)' LAYERS REPETITIONS MIN MIN'
      WRITE(*,*)' 1-6'
      WRITE(*,180)NOMATL,TOTTIM/24.0,TFRQ,TPRNT
      WRITE(*,*)'
      WRITE(*,*)' INITIAL-TEMPERATURE-PROFILE'
      WRITE(*,*)'
      WRITE(*,145)(XXX(J,5),YYY(J,5)-273.15,
& J=1,NIPTS)
      WRITE(*,*)'
      WRITE(*,*)' TOP-SURFACE-CONSTANTS'
      WRITE(*,*)'
      WRITE(*,*)' EMISS ALBEDO '
      WRITE(*,200)EPSN,SMALLA
      WRITE(*,*)'
      WRITE(*,*)' INPUT-LAYER-SPECIFICATIONS'
      WRITE(*,*)' LAYER THICKNESS VERT. GRID THERMAL DIFF HEAT COND'
      WRITE(*,*)' NO. CM SPACE-CM CM**2/MIN'
&   , ' CAL/MIN-CM-K'
      DO 99956 J4=1,NOMATL
      WRITE(*,210)J4,THK(J4),SFRQ(J4),
& ALPH(J4),PK(J4)
99956 CONTINUE
      WRITE(*,*)'
      WRITE(*,*)' INPUT BOTTOM BOUNDARY DATA'
      WRITE(*,*)'
      IF(.NOT.(LFLUXY.EQ.0)) GO TO 99958
      WRITE(*,90)LFLUXY
      WRITE(*,92)DPFM0-273.15
      WRITE(*,*)'
      WRITE(*,*)'

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GO TO 99950
99956 IF(.NOT.(LFLUXY.LT.0)) GO TO 99957
      WRITE(*,90)LFLUXY
      WRITE(*,85)DFMM1*697.6
      WRITE(*,*)'
      GO TO 99958
99957 WRITE(*,90)LFLUXY
      WRITE(*,85)DFMM1*697.6
      WRITE(*,*)'--- BOTTOM SURFACE----- SURFACE BENEATH AIRSPACE TEMP'
      WRITE(*,*)'EMISSIVITY GEOM SHAPE   EMISSIVITY GEOM SHAPE   DEG C'
      WRITE(*,*)'           FACT(0.-1.)           FACT(0.-1.)'
      WRITE(*,97)BEP,BK,REP,BK,TR-273.15
      WRITE(*,*)'
99959 WRITE(*,*)'
      IF(IVEG.EQ.0) GO TO I99988
      WRITE(*,*)' VEGETATION PARAMETERS'
      WRITE(*,*)'
      WRITE(*,*)' COVERAGE      STATE      EMISSIVITY      ALBEDO
& FOLIAGE HEIGHT'
      WRITE(*,*)' (0.0 -1.0)          (0.0 -1.0)          (0.0-1.0)
& (CM)'
      WRITE(*,240)SIGF,STATE,EFF,FOLA,HPOL
      WRITE(*,*)'
      WRITE(*,*)'
      WRITE(*,*)'
      GO TO I99988

C-----
99985 CONTINUE
C     TO CALCULATE-INSOLATION-ON-SLOPE-SURFACE
C
C
C     SOLVE-SOLAR-ZENITH
ASSIGN 99951 TO I99952
GO TO 99952

C
C     SOLVE-SOLAR-AZIMUTH
99951 ASSIGN 99949 TO I99950
GO TO 99950

C
C     CALCULATE-SLOPE-ATMOS-ATTEN-AND-CLOUD-ADJUSTMENTS
99949 ASSIGN 99947 TO I99948
GO TO 99948

C
99947 CONTINUE
C
99953 GO TO I99985
C-----
99955 CONTINUE
C     TO ZERO-VARIABLES
C
      I=0
      GO TO I99955

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```

C-----
99952 CONTINUE
C     TO SOLVE-SOLAR-ZENITH
C
      TIME=AMOD(TIME,24.0)
      T0=2.0*PI*(DAY-1.0)/365.0
      DECL=0.006918-0.399912*COS(T0)+0.070257*SIN(T0)
      & -0.006758*COS(2.0*T0)+0.000907*SIN(2.0*T0)
      & -0.002697*COS(3.0*T0)+0.001480*SIN(3.0*T0)
      ELF=(LAT/180*PI)
      TIMER=(TIME/12*PI)+PI
      IF(TIMER.GT.2.*PI)TIMER=TIMER-2.*PI
      AA=COS(DECL)*COS(ELF)*COS(TIMER)
      BB=SIN(DECL)*SIN(ELF)
      C=AA+BB
      Z=ACOS(C)
      GO TO 199952
C-----
99950 CONTINUE
C     TO SOLVE-SOLAR-AZIMUTH
C
      XNUM=-COS(DECL)*SIN(TIMER)
      XDNUM=COS(ELF)*SIN(DECL)-SIN(ELF)*COS(TIMER)
      SAZ=ATAN(XNUM/XDNUM)
      IF(.NOT.(XNUM.LT.0.0.AND.XDNUM.GT.0.0)) GO TO 99944
      SAZ=SAZ+PI
      GO TO 99945
99944 IF(.NOT.(XNUM.GT.0.0.AND.XDNUM.GT.0.0)) GO TO 99943
      SAZ=SAZ-PI
99943 CONTINUE
99945 GO TO 199950
C-----
99948 CONTINUE
C     TO CALCULATE-SLOPE-ATMOS-ATTEM-AND-CLOUD-ADJUSTMENTS
C
      SICP=COS(Z)*COS(SLOPE)+SIN(Z)*SIN(SLOPE)
      & *COS(SAZ-SURFAC)
      IF(.NOT.(SICP.LT.0.0.OR.COS(Z).LE.0.0)) GO TO 99941
      SUM=0.0
      GO TO 99942
99941 M=1/COS(Z)
      IF(.NOT.(M.GE.0.0)) GO TO 99939
      TAL=0.02023
      IF(DAY.GE.92.0 .AND. DAY.LE.152.0)TAL=-0.02290
      TD=5352.2/(21.4-ALOG(RH*ESAT(TA)))
      WATER=EXP(0.07074*(TD-273.15)+TAL)
      AB=0.271*(WATER**M)**0.303
      AO=0.085-0.247* ALOG10(PRESS/1000.*1./M)
      ARG1=((1.-AB)*0.349+(1.-AO)/(1.-AO*0.2)*0.651)
      GO TO 99940
99939 ARG1=1.0
99940 QF=2.0*ARG1

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```

QQ=QP*SICF
IF(.NOT.(MCLOUD.EQ.0)) GO TO 99937
SUM=QQ
GO TO 99938
99937 CONTINUE
ARG2=-(BCL(MCLOUD)-.059)*M
CTF=(ACL(MCLOUD)/94.4)*EXP(ARG2)
SUM=QQ-((CLOUD*CLOUD)*(QQ-QO*CTF))
99938 CONTINUE
99942 CONTINUE
GO TO 199948
C-----
99943 CONTINUE
C    TO CALCULATE-TABLE-SLOPE-AND-INTERCEPT
I=1
GO TO 99935
99936 IF(I.GT.10) GO TO 99934
99935 IMAX=MAX(I)
IF(IMAX.EQ.0)GO TO 99931
J=1
GO TO 99932
99933 IF(J.EQ.IMAX) GO TO 99931
99932 FMM(J,I)=(YYY(J+1,I)-YYY(J,I))/(XXX(J+1,I)-XXX(J,I))
BBB(J,I)=YYY(J,I)-FMM(J,I)*XXX(J,I)
J=J+1
GO TO 99933
99931 I=I+1
GO TO 99936
99934 GO TO 199948
C-----
99930 CONTINUE
C    TO GET-TABLE-VALUES
C
IMAX=MAX(NTABL)
IJ=1
IF(.NOT.(XN.GE.XXX(IMAX,NTABL))) GO TO 99928
YN=YYY(IMAX,NTABL)
GO TO 99929
99928 IF(IJ.EQ.IMAX+1) GO TO 99927
JJ=IJ
IF(.NOT.(XXX(IJ,NTABL).LT.XN)) GO TO 99925
IJ=IJ+1
GO TO 99928
99925 IF(.NOT.(XXX(IJ,NTABL).EQ.XN)) GO TO 99924
YN=YYY(JJ,NTABL)
IJ=IMAX+1
GO TO 99928
99924 IF(.NOT.(XXX(IJ,NTABL).GT.XN)) GO TO 99923
JJ=JJ-1
YN=FMM(JJ,NTABL)*XN+BBB(JJ,NTABL)
IJ=IMAX+1
99923 CONTINUE

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```
GO TO 99928
99927 CONTINUE
99929 GO TO I99930
C-----
99981 CONTINUE
C      TO CALCULATE-SURFACE-AND-LAYER-TEMPERATURE
C
C      SET-UP-INITIAL-CONDITIONS
ASSIGN 99921 TO I99922
GO TO 99922
C
C      PRINT-OUTPUT-HEADING
99921 ASSIGN 99919 TO I99920
GO TO 99920
C
99919 CONTINUE
C
C      RUN-HEAT-FLOW-PROGRAM
ASSIGN 99917 TO I99918
GO TO 99918
C
C      SET-UP-AND-PRINT-OUTPUT
99917 ASSIGN 99915 TO I99916
GO TO 99916
C
99915 IF(IRETRN.EQ.1) GO TO 4100
GO TO 99919
4100 CONTINUE
GO TO I99981
C-----
99922 CONTINUE
C      TO SET-UP-INITIAL-CONDITIONS
C
PTIME=TOTTIM-24.0
TIME=XXX(1,1)
DIST=0.
IFLAG=0
IF (TFRQ.LE.0) TFRQ=TOTTIM
DELT=TFRQ/60.
ITIME=MAX1(TOTTIM/DELT+.9,1.1)
IX=1
IY=1
GO TO 99913
99914 IF(IX.GT.NOMATL) GO TO 99912
99913 INTR(IX)=IY
IF (SFRQ(IX).LE.0.) SFRQ(IX)=THK(IX)/10.
NX(IX)=MAX1(THK(IX)/SFRQ(IX)+.9,1.1)
RR(IX)=60.0*DELT/(SFRQ(IX)*SFRQ(IX))
C
C CALCULATION OF NUMERICAL STABILITY PARAMETER, TO
C ENSURE NUMERICAL STABILITY.
C
```

```

STABW(IX)=ALPH(IX)*RR(IX)
IF(STABW(IX).GT.0.5)THEN
STABW(IX)=0.5
END IF
C
LAYERS=0
GO TO 99910
99911 IF(LAYERS.GT.NX(IX)) GO TO 99909
99910 XN=DIST
NTABL=5
DEPTH(IY)=XN
C
C      GET-TABLE-VALUES
ASSIGN 99908 TO I99930
GO TO 99930
C
99908 TEMP=YN
STOR(1,IY)=TEMP
STOR(5,IY)=TEMP
STOR(6,IY)=PK(IX)
STOR(7,IY)=RHOC(IX)
STOR(4,IY)=0.
STOR(2,IY)=PK(IX)
STOR(3,IY)=RHOC(IX)
IY=IY+1
DIST=DIST+SFRQ(IX)
LAYERS=LAYERS+1
GO TO 99911
99909 IX=IX+1
DIST=DIST-SFRQ(IX-1)
GO TO 99914
99912 JMAX=IY-1
INTR(IX)=JMAX
NPRINT=MAX1(IPRINT/TFRQ+.9,1.1)
IPRINT=NPRINT
GO TO I99922
C-----
99920 CONTINUE
C      TO PRINT-OUTPUT-HEADING
C
C      IF(OUTCD.EQ.1)GO TO 1610
C      IF(IVEG.GT.0) GO TO 1420
C      WRITE(*,350)
C      WRITE(*,360)
C      WRITE(*,370)
C      WRITE(*,380)
C      GO TO I99920
C1420 WRITE(*,310)
C      WRITE(*,320)
C      WRITE(*,330)
C      WRITE(*,340)
C      GO TO I99920

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```
C1610 WRITE(*,390)
      GO TO I99920
C-----
99918 CONTINUE
C      TO RUN-HEAT-FLOW-PROGRAM
C
IF(.NOT.(IFLAG2.EQ.0)) GO TO 99907
ITER=NIT
TIME=TIME+DELT
99907 ZZA=STOR(5,1)
ZZB=STOR(5,JMAX)
TEML-ZZA
TEMP=ZZB
C
C
C      CALCULATE-BOUNDARY-CONDITIONS
C CALCULATE ENERGY-BUDGET TERMS WITH VEGETATION OR WITHOUT
C
IF(IVEG.EQ.0)GO TO 930
ASSIGN 99905 TO I99900
GO TO 99900
930 ASSIGN 99905 TO I99906
GO TO 99906
C
C      CALCULATE-UPPER-BOUNDARY-VALUES
C USING ENERGY-BUDGET, FIND TOP TEMPERATURE WITH VEGETATION
C OR WITHOUT.
C
99905 IF(IVEG.EQ.0) GO TO 900
ASSIGN 99903 TO I99797
GO TO 99797
900 ASSIGN 99903 TO I99904
GO TO 99904
C
99903 IX=1
J=2
IMATL=NOMATL
IF(.NOT.(NOMATL.EQ.1)) GO TO 99901
IZ=MX(IX)-1
IF(.NOT.(IZ.GT.0)) GO TO 99900
C
C      CALCULATE-INSIDE-MATERIAL-VALUES
ASSIGN 99898 TO I99899
GO TO 99899
C
99898 CONTINUE
99900 GO TO 99902
99901 GO TO 99896
99897 IF(IMATL.LT.1) GO TO 99895
99896 IF(.NOT.(IMATL.GT.1)) GO TO 99893
IZ=MX(IX)-1
IF(.NOT.(IZ.GT.0)) GO TO 99892
```

C  
C     CALCULATE-INSIDE MATERIAL-VALUES  
      ASSIGN 99891 TO I99899  
      GO TO 99899  
C  
99891 CONTINUE  
C  
C     CALCULATE-INTERFACE-VALUES  
99892 ASSIGN 99889 TO I99890  
      GO TO 99890  
99889 GO TO 99894  
99893 IZ=IX(IX)-1  
      IF(.NOT.(IZ.GT.0)) GO TO 99888  
C  
C     CALCULATE-INSIDE-MATERIAL-VALUES  
      ASSIGN 99887 TO I99899  
C  
      GO TO 99899  
99887 CONTINUE  
99888 CONTINUE  
99894 IMATL=IMATL-1  
      GO TO 99897  
99895 CONTINUE  
C  
C     CALCULATE-LOWER-BOUNDARY-VALUES  
99902 ASSIGN 99883 TO I99886  
      GO TO 99886  
C  
99883 GO TO I99918  
C-----  
99906 CONTINUE  
C     TO CALCULATE-BOUNDARY-CONDITIONS  
      B = -PK(1)  
      T-TIME  
C  
C     CALCULATE-BOTTOM-BOUNDARY-HEAT-TERMS-AFRM-DPRM-BPRM  
      ASSIGN 99880 TO I99881  
      GO TO 99881  
C  
C  
C     ATMOSPHERIC-INFRARED-EMISSION-ATERM  
99880 ASSIGN 99878 TO I99879  
      GO TO 99879  
C  
99878 CONTINUE  
C     CALCULATE-SOLAR-INSOLATION-FOR-DAY-AND-TIME  
      DAY=XX(1,8)  
      ASSIGN 42 TO I99885  
      GO TO 99885  
42     BTERM=SUN  
      IF(BTERM.GT.0)BTERM=BTERM\*SMALLA  
C

C      CALCULATE-CONVECTION-BTERM  
ASSIGN 99876 TO I99877  
GO TO 99877

C

C

C      CALCULATE-EVAPORATIVE-HEAT-LOSS-DTERM  
99876 ASSIGN 99874 TO I99875  
GO TO 99875

C

99874 D = ATERM + BTERM - HTERM-DTERM  
521 CONTINUE  
GO TO I99906

C-----

99881 CONTINUE

C      TO CALCULATE-BOTTOM-BOUNDARY-HEAT-TERMS-APRM-DPRM-BPRM

C

BPRM=TB  
IF(.NOT.(TB.EQ.0.0)) GO TO 99872  
APRM=1.0  
DPRM=DPRM0  
GO TO 99873

99872 APRM=FACTZ\*TEMR\*TEMR\*TEMR  
DPRM=DPRM1

99873 GO TO I99881

C-----

99878 CONTINUE

C      TO ATMOSPHERIC-INFRARED-EMISSION-ATERM  
XN=TIME  
NTABL=2

C

C      GET-TABLE-VALUES  
ASSIGN 99887 TO I99930  
GO TO 99930

C

99867 RE=YN  
XN=TIME  
NTABL=10

C

C      GET-TABLE-VALUES  
ASSIGN 99866 TO I99930  
GO TO 99930

C

99866 TA=YN  
XN=TIME  
NTABL=3

C

C      GET-TABLE-VALUES  
ASSIGN 99865 TO I99930  
GO TO 99930

C

99865 CLOUD=YN  
TAK=TA

```

TAC=(TAK-273.15)
EA=6.108*RH*EXP((AC*TAC)/(TAK-BC))
ALPHI=(0.61+0.05*SQRT(EA))*(1.0+(CLR(NCLOUD)*(CLOUD**2)))
DOWNNIR=0.8132E-10*TAK**4*ALPHI
ATERM=DOWNNIR
GO TO I99879
C-----
99877 CONTINUE
C   TO CALCULATE-CONVECTION-HTERM
C
      XN=TIME
      NTABL=6
C
C   GET-TABLE-VALUES
      ASSIGN 99862 TO I99930
      GO TO 99930
C
99862 SPEED=YH
      TAK=TA
      ZASH=ZA
      TSK=TEML
      RHOA=-0.001*0.348*PRESS/TAK
1200 THETAZ=TAK*FACTH
      THETAS=TSK*FACTH
      DTHETA=(THETAZ-THETAS)/ZASH
      DU=SPEED/ZASH
      THETAV=(THETAZ+THETAS)/2.0
      RI=G*DTHETA/(THETAV*DU**2)
      COE1=15.0
      COE2=1.175
      EX=.75
      IF(TSK.GT.TAK)GO TO 31
      IF(RI.GT.0.2)RI=.19999
      COE1=5.0
      COE2=1.0
      EX=2.0
31   HTER=RHOA*KSQ*ZASH**2*DU
      & *(COE2*(1.0-COE1*RI)**EX)
      HTER=HTER*CP*DTHETA
99864 GO TO I99877
C-----
99875 CONTINUE
C   TO CALCULATE-EVAPORATIVE-HEAT-LOSS-DTERM
C
      XN=TIME
      NTABL=2
C
C   GET-TABLE-VALUES
      ASSIGN 99859 TO I99930
      GO TO 99930
C
99859 RH=YH

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```

XN=TIME
NTABL=10

C
C      GET-TABLE-VALUES
ASSIGN 99858 TO I99930
GO TO 99930

C
99858 CTEMA=YH
KTEMPA=CTEMA
CTEMA=CTEMA-273.15
KTEMPG=TEML
ES=EXP((AC*(KTEMPG-273.15))/(KTEMPG-BC))*6.1071
EA=EXP((AC*CTEMA)/(KTEMPA-BC))*6.1071*RH
DG=0.622*PRESS*(EA-ES)*WET/ZA
XL=597.3-0.566*(CTEMA+KTEMPG-273.15)/2.0
DTERM=DTER*DTER*XL*D
GO TO 99861
99860 DTERM=0.0
99861 GO TO I99875
C-----
99904 CONTINUE
C      TO CALCULATE-UPPER-BOUNDARY-VALUES
T1=STABN(1)*(STOR(1,3)-2.*STOR(1,2)+STOR(1,1))+STOR(1,2)
III=0
830 III=III+1
T2=STOR(5,1)**4*FACTA*SFRQ(1)+FK(1)*STOR(5,1)
& -(FK(1)*T1+D*SFRQ(1))
T2=T2/(4.*FACTA*SFRQ(1)*STOR(5,1)**3+FK(1)-SFRQ(1)*DDDT)
STOR(5,1)=STOR(5,1)-T2
TEML=STOR(5,1)

C
C SURFACE TEMPERATURE (TEML, STOR(5,1)) NOT ALLOWED TO RISE
C ABOVE 0 °C. NO ST SNOW PRESENT. THE SNOWPACK IS SATURATED
C AT 0°C AND UNSATURATED AT TEMPERATURES BELOW 0°C.
C
IF(TEML.GE.273.15)THEN
TEML=273.15
WET=1.0
ELSE
WET=0.0
END IF
IF(STOR(5,1).GT.273.15)THEN
STOR(5,1)=273.15
END IF

C
GTERM=-FK(1)*(STOR(5,1)-T1)/SFRQ(1)
ASSIGN 825 TO I99877
GO TO 99877
825 ASSIGN 810 TO I99875
GO TO 99875
810 DNEW=ATERM+BTERM+CTERM-DTERM
IF(ABS(T2).LT.0.005 .OR. III.GT.30)GO TO I99904

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```

DODT--(DNEW-D)/T2
D=DNEW
GO TO 830
C
C-----
99899 CONTINUE
C    TO CALCULATE-INSIDE-MATERIAL-VALUES
C
GO TO 99858
99857 IF(IZ.LE.0) GO TO 99855
99856 CONTINUE
    STOR(5,J)=STOR(1,J)+STABN(IX)*(STOR(1,J-1)-2.*STOR(1,J)
& +STOR(1,J+1))
    J=J+1
    IZ=IZ-1
    GO TO 99857
99855 GO TO I99899
C-
C    TO CALCULATE-INTERFACE-VALUES
C
99890 CONTINUE
    BCOEF=STOR(6,J-1)/SFRQ(IX)
    DCOEF=STOR(6,J+1)/SFRQ(IX+1)
    CCOEF=BCOEF+DCOEF
    ACOEF=BCOEF/(2.*STABN(IX))+DCOEF/(2.*STABN(IX+1))
    STOR(5,J)=STOR(1,J)+(BCOEF*STOR(1,J-1)-CCOEF*STOR(1,J)+DCOEF*
& STOR(1,J+2))/ACOEF
    STOR(5,J+1)=STOR(5,J)
    IX=IX+1
    J=J+2
    GO TO I99890
C-
C    TO CALCULATE-LOWER-BOUNDARY-VALUES
99886 IF(LFLUXY.EQ.0) GO TO 880
    I=1
    R2=FACTD
870 CONTINUE
    R1=SIGMA*BEP*BK*STOR(5,J)**4
    G1=-FK(NOMATL)*(STOR(5,J)-STOR(1,J-1))/SFRQ(NOMATL)
    F2=4.0*SIGMA*BEP*BK*STOR(5,J)**3-FK(NOMATL)/SFRQ(NOMATL)
    F2= -(R2-R1+G1+DPBM)/F2
    STOR(5,J)=STOR(5,J) + F2
    I=I+1
    IF(ABS(F2).GT.0.01 .AND. I.LE.30) GO TO 870
880 IF(LFLUXY.EQ.0) STOR(5,J)=STOR(5,J)
GO TO I99886
C-
99916 CONTINUE
C    TO SET-UP-AND-MANIPULATE OUTPUT
C
    IFLAG2=0
    IRETUR=0

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```

IF(ITER.LE.1) GO TO 1245
ITER=ITER-1
IF (IEPSWT.NE.0) GO TO 1328
IF (IPRNT.LE.1) GO TO 1244
IF (ITIME.GT.1) GO TO 1328
1244 CONTINUE
C
C      MANIPULATE OUTPUT
ASSIGN 99846 TO I99847
GO TO 99847
C
99846 GO TO 1328
1245 IF (ITIME.GT.1) GO TO 1269
C
C      MANIPULATE OUPUT
ASSIGN 99845 TO I99847
GO TO 99847
C
99845 IRETRN=1
GO TO 1335
1269 ITIME=ITIME-1
IF (IPRNT.LE.1) GO TO 1279
IPRNT=IPRNT-1
GO TO 1303
1279 CONTINUE
C
C      MANIPULATE OUTPUT
ASSIGN 99844 TO I99847
GO TO 99847
C
99844 IPRNT=NPRNT
1303 J=1
IZ=NOMATL
1306 IX=NX(IZ)+1
1311 STOR(1,J)=STOR(5,J)
STOR(2,J)=STOR(6,J)
STOR(3,J)=STOR(7,J)
J=J+1
IF (IX.LE.1) GO TO 1329
IX=IX-1
GO TO 1311
1329 IF(IZ.LE.1) GO TO 1335
IZ = IZ-1
GO TO 1306
1328 IFLAG2=1
1335 CONTINUE
GO TO I99918
C-----
99847 CONTINUE
C OUTPUT MANIPULATION
C HOURLY ENERGY VALUES FOR BOTH UNVEGETATED AND UNVEGETATED SURFACES
C ARE CONVERTED INTO lyhr-1. THE ENERGY VALUES, SURFACE AND BASAL

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C TEMPERATURES AND CORRESPONDING HOUR OF THE DAY ARE PLACED IN A DATA
C MATRIX, DATMX.
C
      TFACK=1.0
      IF(.NOT.(TIME.GT.PTIME)) GO TO 99843
      DO 99842 JKK=1,NOMATL+1
      IJ=INTR(JKK)
      TITLE(JKK)=(STOR(5,IJ)-273.15)
99842  CONTINUE
      NDX=TIME
      IF(NDX.EQ.0)NDX=1
C
C RESULTS CALCULATED IN  $\text{calcm}^{-2}\text{min}^{-1}$  IE.  $\text{lymin}^{-1}$  AND
C CONVERTED TO  $\text{lyhr}^{-1}$  BY *60. THE DAILY TOTAL IS THEN DIVIDED
C BY 24 (ELSEWHERE IN THE PROGRAM) TO HAVE ANSWER IN  $\text{MJm}^{-2}\text{day}^{-1}$ .
C  $\text{MJm}^{-2}\text{day}^{-1}$ . IS NOW THE MORE WIDELY USED UNIT AND THEREFORE IS
C USED.
C
      STP=TITLE(1)
      BOTTP=STOR(5,J)-273.15
      K10=K10+1
      IF(IVEG.EQ.1) GO TO 1110
C
C ENERGY VALUES FOR UNVEGETATED SURFACE, CONVERTED TO  $\text{lyhr}^{-1}$ .
C
      IBGR=(0.813E-10*EPSN*STOR(5,1)**4)*60
      ISOL=(BTERM/SMALLA)*60
      IABSOR=(ISOL*SMALLA)
      IATERM=ATERM*60
      ITERM=BTERM*60
      IDTERM=DTERM*60
C
      1110  CONTINUE
      DATMX(K10,1)=TIME
      DATMX(K10,2)=TITLE(1)
C
C CALCULATE VEGETATION RADIANCE VALUES IF VEGETATION MODELLED
C
      ASSIGN 1400 TO I1410
      IF(IVEG.EQ.1) GO TO 1410
1400  CONTINUE
C
      IF(IVEG.EQ.0)THEN
C*****OPTION 2-HOURLY VALUES FOR ENERGY-BUDGET VALUES.
C INSERT:
      WRITE(9,190)AMOD(TIME,24.),TITLE(1),IBGR,ISOL,IABSOR,
      & IATERM,ITERM,IDTERM
C*****
C
      DATMX(K10,3)=IBGR
      DATMX(K10,4)=ISOL

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```

DATMX(K10,5)=IABSOR
DATMX(K10,6)=IATERM
DATMX(K10,7)=INTERM
DATMX(K10,8)=IDTERM
DATMX(K10,9)=BOTTP
ELSE
C*****
C OPTION 2-HOURLY VALUES FOR ENERGY-BUDGET VALUES.
C INSERT:
      WRITE(9,270)AMOD(TIME,24.),ISURFG+IREFRA,ISURFG,
      & TEFFR-273.15,TEFF-273.15,TEML-273.15,TF-273.15,ISOL,SG
C*****
C
      DATMX(K10,3)=GRNDGB*60
      DATMX(K10,4)=SG
      DATMX(K10,5)=IABSOR
      DATMX(K10,6)=RLD*60
      DATMX(K10,7)=ESG*60
      DATMX(K10,8)=ELG*KL1*60
      DATMX(K10,9)=BOTTP
      END IF
99843 GO TO I99847
C-----
99800 CONTINUE
C      TO CALCULATE-BOUNDARY-CONDITIONS-WITH-VEG
      T=TIME
      XN=TIME
      NTABL=6
C
C      GET-TABLE-VALUES
      ASSIGN 960 TO I99930
      GO TO 99930
C
      960 UA=YN
      XN=TIME
      NTABL=4
C
C      ATMOSPHERIC-INFRARED-EMISSION-ATERM
      ASSIGN 960 TO I99879
      GO TO 99879
C
C      CALCULATE INCOMING SOLAR RADIATION.
      960 CONTINUE
      DAY=XXX(1,8)
      ASSIGN 43 TO I99985
      GO TO 99985
      43 SOL=SUN
C
      IF(UA.LT.10.0)UA=10.0
      UAF=0.83*SIGF*UA*SQRT(CHE)+(1.-SIGF)*UA
      DELTMR=5.
      CF=0.01*(1.+30.0/UAF)

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```

DU=(UA-UAF)/ZA
RS=1/(.05+.0021*(SOL=60))
RC=RS*STATE/(7.0*SIGF)
ATF(1)=TF
ASSIGN 1210 TO I950
GO TO 950
1210  CONTINUE
FEB(1)=FENB
NDEX=0
1240  TF=TF+DELTMP
NDEX=NDEX+1
ASSIGN 1220 TO I950
GO TO 950
1220  CONTINUE
IF(NDEX.EQ.3.AND.FENB.LT.0.0)THEN
FEND=FENB*(-1.0)
END IF
FEB(2)=FENB
IF(FEB(1)*FEB(2).LT.0.0) GO TO 1230
IF(NDEX.EQ.5)THEN
GOTO 1230
END IF
IF(ABS(FEB(2)).GT.ABS(FEB(1)))DELTMP=-5.
IF(NDEX.LT.100)GO TO 1240
WRITE(*,*)'POLIAGE ENERGY BUDGET HAS NOT CROSSED X-AXIS'
WRITE(*,*)'AFTER 100 SEARCH STEPS. CHECK INPUT DATA.'
STOP
1230  CONTINUE
NDEX1=0
ATF(2)=TF
1270  SLOPE2=(FEB(2)-FEB(1))/(ATF(2)-ATF(1))
BINT=FEB(1)-SLOPE2*ATF(1)
TFO=-BINT/SLOPE2
NDEX1=NDEX1+1
IF(ABS(TF-TFO).LE.0.01)GO TO 1260
IF(NDEX1.EQ.5)THEN
GOTO 1260
END IF
TF=TFO
ASSIGN 1250 TO I950
GO TO 950
1250  CONTINUE
IF(FENB>FEB(2).GT.0.0)IP=2
IF(FENB>FEB(1).GT.0.0)IP=1
ATF(IP)=TF
FEB(IP)=FENB
GO TO 1270
1260  GO TO I99800
C-----  

C      TO CALCULATE-UPPER-BOUNDARY-VALUES-FOR-POLIAGE
99797  CONTINUE
DELTMP=5.

```

```

ATF(1)=TEM1
ASSIGN 1310 TO I1300
GO TO 1300
1310  CONTINUE
FEB(1)=FENB
NDEX=0
1340  TEM1=TEM1+DELTMP
NDEX=NDEX+1
ASSIGN 1320 TO I1300
GO TO 1300
1320  CONTINUE
FEB(2)=FENB
IF(FEB(1)*FEB(2).LT.0.0) GO TO 1330
IF(NDEX.EQ.5)THEN
GOTO 1330
END IF
IF(ABS(FEB(2)).GT.ABS(FEB(1)))DELTMP=-5.
IF(NDEX.LT.100)GO TO 1340
WRITE(*,*)'GROUND ENERGY BUDGET HAS NOT CROSSED X-AXIS'
WRITE(*,*)'AFTER 100 SEARCH STEPS. CHECK INPUT DATA.'
STOP
1330  CONTINUE
NDEX1=0
ATF(2)=TEM1
1370  SLOPE2=(FEB(2)-FEB(1))/(ATF(2)-ATF(1))
BINT=FEB(1)-SLOPE2*ATF(1)
TF0=-BINT/SLOPE2
NDEX1=NDEX1+1
IF(ABS(TEM1-TF0).LE.0.001)GO TO 1360
IF(NDEX1.EQ.5)THEN
GOTO 1360
END IF
TEM1=TF0
ASSIGN 1350 TO I1300
GO TO 1300
1350  CONTINUE
IF(FENB*FEB(2).GT.0.0)IP=2
IF(FENB*FEB(1).GT.0.0)IP=1
ATF(IP)=TEM1
FEB(IP)=FENB
GO TO 1370
1360  STOR(5,1)=TEM1
IF(TEM1.GE.273.15)THEN
TEM1=273.15
END IF
GO TO 199797
C-----
C      TO CALCULATE-ENERGY-BUDGET
950  TAP=(1.-SIGF)*TA+SIGF*(0.3*TA+0.6*TF+0.1*TEM1)
DTHEETA=(TA-TF)*FACTH/ZA
THETAV=(TA+TF)*FACTH/2.0
RI=G*DTHEETA/(THETAV*DU**2)

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RHOAF=0.001*.348*PRESS/((TF+TA)/2.)
COE1=15.
COE2=1.175
EX=.75
IF(RI.LE.0.)GO TO 1280
IF(RI.GT.0.2)RI=0.199
COE1=5
COE2=1.
EX=2.0
1280 CONTINUE
HTER=RHOAF*KSQ*ZA**2*DU
& *COE2*(1.-COE1*RI)**EX
HSF=HTER*CP*DTHETA*60.
XL=597.3-0.566*TAF
RA=( ALOG((ZA-ZDSP)/Z0)*COE2*((1.-COE1*RI)**EX))**2
& /(.18*UA)
RDP=RA/(RS+RA)
QF=RDP*QSAT(TP)+(1.-RDP)*QAF
QAF=(1.-SIGF)*Q(TA)+SIGF*(Q(TA)*0.3+QF*0.6+QG*0.1)
LF=(RHOAF*CP/0.66)*(ESAT(TP)-E(TA))/(RA+RC)*60.
IF(EF.LT.0.0)EF=0.0
SHRF=POLA*SOL
XLNG=EFF*ATERM
TG4=EFF*EPSN/EP1*SIGMA*TEML**4
TF4=(EP1+EPSN)/EP1*EFF*SIGMA*TF**4
FEND=SIGF*(SHRF+XLNG+TG4-TF4)-HSF-EF
GO TO 1950
C-----
C TO CALCULATE-ENERGY-BUDGET-FOR-GROUND
1300 CONTINUE
T1=ALPH(1)*RR(1)*(STOR(1,3)-2.*STOR(1,2)+STOR(1,1))
& +STOR(1,2)
TF4=SIGMA*TF**4
TG4=SIGMA*TEML**4
QG=WET*QSAT(TEML)+(1.-WET)*QAF
RHOAG=0.001*0.348*PRESS/TAF
XL1=597.3-0.566*(TAF+TEML-2.0*273.15)/2.
SG=(1.-SIGF)*SOL
RLU=(1.-SIGF)*(EPSN*TG4+(1.-EPSN)*ATERM)
& +SIGF*(EPSN*TG4+(1.-EPSN)*EFF*TF4)/EP1
RLD=(1.-SIGF)*ATERM+SIGF*(EFF*TF4+(1.-EFF)*EPSN*TG4)/EP1
HSG=RHOAG*CP*CHG*UAF*(TEML-TAF)*60.
ELG=RHOAG*CHG*UAF*(QG-QAF)*60.
FEND=SMALLA*SG-RLU+RLD-HSG-ELG*XL1+(T1-TEML)/SFRO(1)*FK(1)
GO TO 11300
C-----
C TO CALCULATE-RADIANCE-VALUES
1410 CONTINUE
REFRAD=((1.-SIGF)*(1-EPSN)+SIGF*(1-EFF))*DOWNIR
POLGB=EFF*0.8132E-10*TF**4
GRNDGB=EPSN*0.8132E-10*TEML**4
SURFGB=SIGF*POLGB+(1.-SIGF)*GRNDGB

```

```
EFP=SIGF*EFF+(1.-SIGF)*EPSN  
TEFF=(SURPGB/0.8132E-10)**.25  
ISURPG=SURPGB*60  
TEFFR=(((SURPGB+REFRAD)/(0.8132E-10))**.25)  
IREFRA=REFRAD*60  
ISOL=SOL*60  
SG=((1.0-SIGF)*SOL)*60  
IABSOR=SMALLA*SG  
GO TO 11410  
C -----  
END
```

```

*****
C OPTION 3-MASS CONSERVATION ROUTINE
C
C FOR A 2-LAYER PACK
3001   DELRNS=(DELQM/(LHEATP*VNEWSN(1,6)*1000))*100
        IF(DELRNS.GT.0.0)THEN
          IF(DELRNS.GE.THKMK2(1,1))THEN
            ABC=DELRNS-THKMK2(1,1)
            DFG=THKMK2(1,1)
            THKMK2(1,1)=0.0
            DELQM=(ABC*LHEATP*(VNEWSN(1,6)*1000))/100
            DELROS=(DELQM/(LHEATP*(VOLDSN(1,6)*1000)))*100
            IF(DELROS.GE.THKMK2(2,1))THEN
              GOTO 5002
            ELSE
              THKMK2(2,1)=THKMK2(2,1)-DELROS
              DEPTH=THKMK2(2,1)
              NOMATL=1
              NIPTS=2
              DO 800 J=1,5
                THKMK1(J)=VOLDSN(1,J)
800           CONTINUE
                THKMK1(1,1)=DEPTH
                DEPMK1(1,2)=AVSTP
                DEPMK1(2,2)=AVBOTTP
                DEPMK1(2,1)=DEPTH
                GOTO 5000
              END IF
            ELSE
              THKMK2(1,1)=THKMK2(1,1)-DELRNS
              DEPMK2(1,2)=AVSTP
              DEPMK2(3,2)=AVBOTTP
              DEPMK2(3,1)=DEPTH
              DEPMK2(2,1)=THKMK2(1,1)
              DEPMK2(2,2)=((DEPMK2(2,1)/DEPTH)*(AVBOTTP-AVSTP))+AVSTP
              GOTO 5000
            END IF
          ELSE
            GOTO 5000
          END IF
        C
        C FOR A 1-LAYER PACK
4000   IF(THKMK1(1,6).EQ.VNEWSN(1,6))THEN
          DELRNS=(DELQM/(LHEATP*(VNEWSN(1,6)*1000)))*100
          IF(DELRNS.GT.0.0)THEN
            IF(DELRNS.GE.THKMK1(1,1))THEN
              GOTO 5002
            ELSE
              THKMK1(1,1)=THKMK1(1,1)-DELRNS
              DEPTH=THKMK1(1,1)
              DEPMK1(1,2)=AVSTP
              DEPMK1(2,2)=AVBOTTP
            END IF
          ELSE
            GOTO 5000
          END IF
        END IF
      END IF
    END IF
  END IF
END IF

```

```

DEPMX1(2,1)=THKMX1(1,1)
GOTO 5000
END IF
ELSE
GOTO 5000
END IF
ELSE
DELROS=(DELQM/(LHEATF*(VOLDSN(1,6)*1000)))*100
IF(DELROS.GT.0.0)THEN
IF(DELROS.GE.THKMX1(1,1))THEN
GOTO 5002
ELSE
THKMX1(1,1)=THKMX1(1,1)-DELROS
DEPTH=THKMX1(1,1)
DEPMX1(1,2)=AVSTP
DEPMX1(2,2)=AVBOTTP
DEPMX1(2,1)=THKMX1(1,1)
GOTO 5000
END IF
ELSE
GOTO 5000
END IF
END IF

C
5000 IF(NOMATL.EQ.2.AND.THKMX2(1,1).LT.1.0)THEN
DEPTH=THKMX2(1,1)+THKMX2(2,1)
NOMATL=1
NIPTS=2
DO 450 J=1,6
THKMX1(1,J)=VOLDSN(1,J)
450 CONTINUE
THKMX1(1,1)=DEPTH
DEPMX1(2,1)=DEPTH
DEPMX1(1,2)=AVSTP
DEPMX1(2,2)=AVBOTTP
END IF

C
MRSN=DPG+DELROS
WENS=DPG*VNEWSN(1,6)
WEOS=DELROS*VOLDSN(1,6)
MRWE=WENS+WEOS
IF(MRSN.LT.0.0)THEN
MRSN=0.0
END IF
IF(MRWE.LT.0.0)THEN
MRWE=0.0
END IF
*****
```

## VARIABLE DEFINITIONS: SNOMD

## (1) MAIN PROGRAM

AIRTP	Air temperature, °C.
AVABSR	Mean daily shortwave radiation absorbed at the surface, $MJm^{-2} day^{-1}$ .
AVATER	Mean daily shortwave radiation absorbed at the surface, $MJm^{-2} day^{-1}$ .
AVBTTP	Mean daily temperature at the base of the snowpack, °C.
AVDTER	Mean daily evaporative heat flux, $MJm^{-2} day^{-1}$ .
AVGBR	Mean daily reflected longwave radiation, $MJm^{-2} day^{-1}$ .
AVHTER	Mean daily sensible heat flux, $MJm^{-2} day^{-1}$ .
AVSOL	Mean daily incoming shortwave radiation, $MJm^{-2} day^{-1}$ .
AVSTP	Mean snow temperature, °C.
BOTTP	Temperature at the base of the snowpack, °C.
CELL	Identification number of the computational cell being modelled.
CRITDP	Critical snowdepth, 5cm.
DATMX	Matrix holding TSTM output values for manipulation.
DAY	Julian date of day being modelled.
DAY1	Julian date of SNOMD initiation.
DDATE	Julian date of day being modelled.
DELOS	$\Delta Q_s$ , snowpack internal energy change, $MJm^{-2} day^{-1}$ .
DENSN	Density of snow, $g cm^{-3}$ .
DENW	Density of water, $g cm^{-3}$ .
DEPMX1	Depth matrix for a 1-layer pack.
DEPMX2	Depth matrix for a 2-layer pack.
DEPTH	Snowpack depth, cm.
DEPTH1	Used in calculation of depth when converting 'new snow' to 'old snow'.
DUDT	$dU/dt$ , part of the snowpack energy-budget equation (equivalent to $\Delta Q_s$ ), redundant.

ENAVM	Energy available for melt, $\Delta Q_m$ , calculated using energy totals, $MJm^{-2} day^{-1}$ .
GTERM	Ground heat flux, $calcm^{-2} min^{-1}$ .
HCAPSN	Heat capacity of snow, $kJkg^{-1} C^{-1}$ .
HCAPW	Heat capacity of water, $kJkg^{-1} C^{-1}$ .
ILAPSE	Determines which elevation data file is used to modify the air temperatures with lapse rate.
IRAIN	Indicates occurrence of rain-on-snow. If irain=0 then no rain-on-snow occurred, if irain=1 rain-on-snow occurred.
ISNOW	Indicates if snowed on the previous day, isnow=0, no snowfall on previous day, isnow>0, snowfall on previous day.
IVEG	Determines whether VEGIE is activated or not and which vegetation input file is used.
K1	Count of the number of days modelled, ie. the number of times the 'do 5001' loop is used.
K2	K2=0 indicates that SNOMO modelled soil in the previous iteration or that SNOMO is not modelling the first iteration. K2=1 indicates that that SNOMO modelled snow in the previous iteration or that it is the first iteration.
K3	K3=0, indicates soil modelled in previous iteration, K3=1, indicates snow modelled in previous iteration.
K25	Count of the days elapsed since the last snowfall.
K30	Indicator to facilitate the calculation of xsntp, in the melt calculations.
KELVIN	Air temperature converted to degrees kelvin.
KONTRL	Count of the number of days modelled.
LHEATF	Latent heat of fusion, $MJkg^{-1}$ .
MRSW	Meltrate, $cm snow.day^{-1}$
MRME	Meltrate, $mm snow water equivalent.day^{-1}$ .
NETRAD	Net radiation, $m^{-2} day^{-1}$ .

NIPTS	The number of times the output time print frequency is divisible by the time steps, used to determine when to print output.
EKONT	Used with KONTROL to terminate SNOMD.
NOMATL	The number of material layers used in solving the heat flow.
PPTN	Precipitation, mm water.
PTERM	Heat input to pack by rain-on-snow, $MJm^{-2} day^{-1}$ .
RH	Relative humidity, %.
SNDP1	Initial snowdepth, cm
SNPPTN	Precipitation amount, cm snow.
SNVOL	area x depth, $m^{-3}$ .
SOILDP	depth of soil profile at the base of the snowpack, cm.
SOILTP	Soil temperature at depth, taken at soildp, °C.
SPHTI	Specific heat of ice, $2.10 \times 10^3 \text{ J kg}^{-1} \text{ K}^{-1}$ .
SPHTW	Specific heat of water, $4.18 \times 10^3 \text{ J kg}^{-1} \text{ K}^{-1}$ .
SSOLTP	Surface soil temperature, °C.
STP	Surface temperature, °C.
TABSOR	Total daily shortwave radiation absorbed at the surface, $MJm^{-2} day^{-1}$ .
TATERM	Total daily incoming longwave radiation, $MJm^{-2} day^{-1}$ .
TDTERM	Total daily evaporative heat flux, $MJm^{-2} day^{-1}$ .
TGBR	Total daily reflected radiation, $MJm^{-2} day^{-1}$ .
THMX1	Thickness matrix for a 1-layer pack.
THMX2	Thickness matrix for a 2-layer pack.
THTERM	Total daily sensible heat flux, $MJm^{-2} day^{-1}$ .
TIME2	Daily observation time, used to aid the sequential reading of the daily observation time.
TMAX	Lapse rate alteration of the maximum daily air temperature.
TMIN	Lapse rate alteration of the minimum daily air temperature.
TSOL	Total daily incoming solar radiation, $MJm^{-2} day^{-1}$ .

**VNEWSN** Vector holding new snow values of thermal diffusivity, heat conductivity, emissivity, albedo and density.  
**VOLDSN** Vector holding old snow values of thermal diffusivity, heat conductivity, emissivity, albedo and density.  
**VSOIL** Vector holding soil values of thermal diffusivity, heat conductivity, emissivity, albedo and density (redundant).  
  
**WE1** Used in the calculation of depth when converting 'new snow' to 'old snow', cm.  
  
**XXX(J,8)** Julian date.  
**XXX(J,1)** Observation time.  
  
**YEAR** Year of the simulation data.  
**YYY(J,1)** Minimum air temperature, °C, table 1.  
**YYY(J,2)** Relative humidity, %, table 2  
**YYY(J,3)** Cloud cover, 0-1, table 3.  
**YYY(J,6)** Wind speed,  $\text{ms}^{-1}$ , table 6.  
**YYY(J,7)** Precipitation, mm water.  
**YYY(J,9)** Maximum air temperature, °C.

## (2) TSTM

**AB** Mugge-Miller absorption function.  
**ACL(8)** Coefficient, a, dependent on cloud type, used in the calculation of CTF.  
**ALPH(IX)** Thermal diffusivity of layer IX,  $\text{cm}^2 \text{min}^{-1}$ .  
**AO** Atmospheric albedo for Rayleigh scattering.  
**APRM**  $\text{FACTE} * \text{TEMP}^3$ ,  $\text{calcm}^{-2} \text{min}^{-1} \cdot ^\circ\text{C}$ .  
  
**B** Heat conductivity of surface,  $\text{calcm}^{-2} \text{min}^{-1} \cdot ^\circ\text{C}$ .  
**BBB(J,1)** Y intercept of linear equation, used for table interpolation.  
**BC** Constant used in the calculation of water vapour pressure.  
**BCV(8)** Coefficient, b, dependent on cloud type, used in the calculation of CTF.  
**BEP** Bottom boundary thermal IR emissivity.

BK	Bottom surface geometric shape, fraction (0.0-1.0)
BPRM	Heat conductivity of bottom boundary layer.
DTERM	Energy contributed by insolation after adjustment using surface absorptivity, calcm <sup>-2</sup> min <sup>-1</sup> .
CC	CLOUD * CLOUD.
COE1	Coefficient used in the calculation of HTERM, DTERM, EF and DTERM, set according to Richardson's Number.
COE2	Coefficient used in the calculation of HTERM, DTERM, EF and DTERM, set according to Richardson's Number.
COEF	Part of calculation of interface values.
CLR(8)	Coefficient dependent on cloud type, used in the calculation of incoming longwave radiation.
CLOUD	Cloud cover, fraction (0.1-1.0).
CP	Specific heat of dry air at constant pressure.
CTEMA	Air temperature in degrees kelvin, used in calculation of evaporative heat flux.
CTF	Cloud adjustment factor.
DAY	Julian day used in solving insolation.
DCOEF	Part of calculation of interface values.
DDDT	dT/dTg, part of upper boundary calculation.
DECL	Solar declination angle.
DELT	Time step in hours.
DEPTH(IY)	Matrix holding layer depths.
DEPTH(450)	Depth of snow or soil profile.
DOWNIR	Incoming longwave radiation, calcm <sup>-2</sup> min <sup>-1</sup> .
DPRM	Heat flux, calcm <sup>-2</sup> min <sup>-1</sup> , at bottom boundary or temperature in rankines at bottom boundary.
DPRM0	Temperature of bottom material, °C, used when LFLUX=0.
DPRM1	Heat flux of beneath bottom material, calcm <sup>-2</sup> min <sup>-1</sup> , used when LFLUXY not equal 0.
DTERM	Energy flux due to evaporation.
EA	Water vapour pressure of the air.
ELF	Latitude, radians.

EPSN	Emissivity of surface material.
ES	Water vapour pressure of the surface.
ESAT(T)	Saturated vapour pressure at temperature T.
E(T)	Vapour pressure at temperature T.
F2	Part of the calculation of bottom boundary values.
FACTA	$\text{SIGMA} \cdot \text{EPSN}$
FACTD	$\text{FACTD} = \text{SIGMA} \cdot \text{BK} \cdot \text{BEP} \cdot \text{TR}^{**4}$ , used in bottom boundary calculation when there is airspace beneath the bottom layer.
FACTE	$\text{FACTE} = \text{SIGMA} \cdot \text{BK} \cdot \text{BEP}$ , used in bottom boundary calculation when there is airspace beneath the bottom layer.
FACTH	$\text{FACTH} = (1000.0 / \text{PRESS})^{**0.286}$ , used in solving convection term (HTERM).
FK(IX)	Heat conductivity of layer IX, $\text{cal min}^{-1} \text{cm}^{-1} \text{K}^{-1}$ .
FMM(J,I)	Slope of linear equation, used for table interpolation.
G	Acceleration due to gravity.
GTERM	Ground heat flux, $\text{cal cm}^{-2} \text{min}^{-1}$ .
HEADER	72 character input variable used to print comments on output (not utilised in SNOMO).
HTERM	Energy loss or gain due to convection, $\text{cal cm}^{-2} \text{min}^{-1}$ .
IEFSWT	Switch, when =0 will print output only at specified time, if not =0 will print output at every iteration.
IEOF	Set from 0 to 1 when an EOF is encountered, used to terminate program.
III	Count of number of interval iterations in calculation of upper boundary values.
IMATL	Backward counter of layers, starting with the number of layers.
INTR(IX)	Beginning sub-layer depth number for layer number IX.
IPRNT	Backward counter SET+NPRNT. When =1 output is printed.
ITER	Iteration counter used in finite difference calculation of heat flow equation.
ITIME	Backward counter initialize as total time steps in hour.
IX	Layer number starting with top layer.
IY	Sub-layer depth number.

JMAX	The total number of sub-layers.
K10	Count of the number of internal iterations of TSTM, in order to calculate the daily means of the TSTM calcuated energy-budget and temperature variables.
KSQ	von Karman's constant squared.
KTEMPA	Air temperature, degrees kelvin.
KTEMPG	Surface temperature, degrees kelvin.
LAYERS	Count of the profile layers.
LAT	Latitude used in solving insolation.
LFLUXY	Input bottom boundary data control switch. If =0, there is no heat flux through bottom of material, if negative there is no air space beneath bottom material, if positive there is air space beneath bottom material.
LN	Dummy variable to read line number from input file.
M	Secant of solar zenith angle, radians.
MAX(J)	Number of input table values used in table interpolation module.
NCLOUD	Cloud type index number (1-9) used in solving insolation, IR emission.
NETRAD	Net radiation, $\text{MJ m}^{-2} \text{day}^{-1}$ .
NIT	Number of iterations used in heat flow calculations.
NKONT	Used with KONTRL to terminate SNOMO.
NTABL	Table number.
NX(IX)	NX(IX)=THK(IX)/SFRQ(IX), number of sublayer of each layer.
OUTCD	Output manipulation variable.
PI	3.141593
PRESS	Atmospheric pressure, mb, used in solving insolation.
PTIME	Beginning time of output=total number of hours minus 24, used in print output module 2.
QSAT(T)	Saturated specific humidity at temperature T.
Q(T)	Specific humidity at temperature T.

REP	Emissivity beneath airspace.
RHOA	Air density, calculated as part of sensible heat calculation.
RHOC(IX)	$\text{FK(IX)}/\text{ALPH(IX)}$ , $\text{calcm}^{-2}\cdot\text{K}^{-1}$ .
RI	Richardson's Number, index used in solving HTERM, DTERM, HTER, EF.
RK	Surface beneath airspace geometric shape, fraction (0.0-1.0).
RR(IX)	$\text{RR(IX)}=\text{DELT}/\text{SFRQ}^{**2}$ , part of heat flow equation.
SAZ	Solar azimuth, radians.
SCF	Used in calculation of sensible heat flux, determined by the Richardson number.
SFRQ(IX)	Vertical grid spacing in cm in each layer IX, $\text{cm}^2\text{m}^{-1}$ .
SICF	Insolation adjustment due to zenith angle, surface slope and surface aspect angle.
SIGMA	Stefan-Boltzman constant, 8.12e-11.
SLOPE	Surface slope, degrees, with horizontal =0 degrees, used in solving insolation.
SMALLA	Absorbtivity of surface material.
SPEED	Wind speed, $\text{cmsec}^{-1}$ .
STABN	Numerical stability parameter, ≤0.5 for numerical stability.
STOR(1,IY)	Estimate sub-layer temperature, degree rankine.
STOR(2,IY)	$\text{FK}$ , heat conductivity of sub-layer IY, $\text{calmin}^{-1}\text{cm}^{-1}\text{K}^{-1}$ .
STOR(3,IY)	$\text{RHOC}$ , $\text{FK}/\text{ALPH}$ , $\text{calcm}^{-2}\cdot\text{K}^{-1}$ .
STOR(4,IY)	Constant dimensionless.
STOR(5,IY)	Initial snow temperature, degree rankine, of initial snow profile.
STOR(6,IY)	Same as STOR(2,IY).
STOR(7,IY)	Same as STOR(3,IY).
SUMC	Count of daily energy totals.
SUN	Calculated insolation value.
SURFAC	Surface azimuth, degrees, with south =0, west =+90 and east =-90 degrees, used in solving insolation.
T	Same as TIME.
TA	Air temperature, degrees rankine.
TAC	Air temperature, °C.
TAK	Air temperature, °K.
TAL	Constant used in the calculation of WATER.

TB Thermal conductivity of bottom material,  $\text{cal cm}^{-2} \cdot \text{C}^{-1} \cdot \text{min}^{-1}$ .

TD Dew point temperature used in the calculation of WATER.

TEML Surface temperature of material, degrees rankine.

TEMR Bottom layer temperature of material in degrees rankine.

TFRQ Time step in minutes used in solving heat flow.

THK(IX) Layer thickness, in cm of layer IX.

TIME Time in hours which material temperatures are estimated.

TIMER Sun's hour angle, radians.

TITLE Surface temperature, °C.

TOTTIM Total number of 24 hour repetitions used in solving heat flow.

TPRNT Output time print frequency, minutes.

TR Temperature of airspace beneath bottom material.

TSK Material sub-layer temperature, °K.

TIME Time in hours, used in insolation calculation.

WATER The amount of precipitable water, mm, used in solving insolation.

WET Moisture content of surface material.

XXX(J,1) Time in hours for table 1 (air temperature).

XXX(J,2) Time in hours for table 2 (relative humidity).

XXX(J,3) Time in hours for table 3 (amount of cloud cover).

XXX(J,4) Time in hours for table 4 (solar insolation).

XXX(J,5) Depth, cm, for table 5 (temperature profile) initial temperature profile, °C.

YYY(J,4) Insolation,  $\text{cal cm}^{-2} \cdot \text{min}^{-1}$ , if 0.0 at 1200 hours, insolation values will be calculated, table 4.

Z Solar zenith angle.

ZA Shelter height, cm.

ZASH Shelter height, cm.

ZZA Surface temperature of material, degree rankine.

ZZB Bottom layer temperature of material in degree rankine.

## (3) VEGIE

ATERM	Atmospheric IR emission, $\text{cal cm}^{-2} \text{min}^{-1}$ .
ATF(1)	Part of the root-finding algorithm.
ATF(2)	Part of the root-finding algorithm.
BINT	Part of the root-finding algorithm.
CHO	Dimensionless heat or moisture transfer coefficient applicable to the top of a dense canopy.
CHE	Dimensionless heat or moisture transfer coefficient applicable to the top of a dense canopy.
CBG	Heat transfer coefficient equation interpolated between ground with no cover, CHO and complete cover, CHE.
CP	Specific heat of dry air at constant pressure.
DELTMP	Incremental temperature for the root-finding algorithm.
DTHETA	$DTHETA = (TA - TF) * FACTH / ZA$ , used in the calculation of the Richardson Number.
DU	Used in the calculation of the Richardson Number.
E(T)	Vapour pressure at temperature T.
EF	Latent heat loss to the atmosphere for the foliage.
EFF	Effective temperature.
ELG	Latent heat loss to the atmosphere at the ground surface.
EP1	Part of the calculation of the energy budget for foliage.
EPF	Emissivity of foliage.
EPSN	Emissivity of ground (snowpack) surface.
ESAT(T)	Saturated vapour pressure at temperature T.
EX	Coefficient used in the calculation of HTERM, DTERM, HTER and EF, set according to Richardson's Number.
FACTH	Potential temperature.
FEB(1)	Part of the root-finding algorithm.
FEB(2)	Part of the root-finding algorithm.

FENB	Energy-budget of the ground and foliage surfaces respectively.
FK(IX)	Heat conductivity of ground (snowpack).
POLA	Absorptivity of the foliage layer (1-albedo).
POLGB	Foliage thermal IR emittance, $\text{calcm}^{-2}\text{min}^{-1}$ .
G	Acceleration due to gravity.
GRNDGB	Ground thermal IR emittance, $\text{calcm}^{-2}\text{min}^{-1}$ .
HPOL	Foliage height, cm.
HSF	Convective energy flux across the foliage surface.
HSG	Convective energy flux across the ground (snowpack) surface.
HTER	Part of the calculation of HSF.
QAF	Specific humidity of air within the foliage layer.
QF	Specific humidity of the air at foliage height.
QG	Specific humidity of the ground (snowpack) surface.
QSAT(T)	Saturated specific humidity at temperature T.
NDEX	Count of the number of times the energy-budget for the ground or the foliage was calculated.
RA	Atmospheric resistance.
RC	Canopy resistance to water vapour diffusion
RDF	Fraction of potential evaporation rate from foliage.
REPRAD	Surface related radiation, $\text{calcm}^{-2}\text{min}^{-1}$ .
RHOAF	Density of air near ground surface.
RHOAG	Density of air near the ground surface.
RI	Richardson Number.
RLD	Downward longwave flux over ground (snowpack) surface.
RLU	Upward directed longwave flux radiated from ground (snowpack) surface.
RS	Stomatal resistance.
SFRQ(IX)	Distance of first grid point below the surface.
SG	Incoming solar radiation reaching the ground (snowpack).

SHEW	Amount of shortwave radiation absorbed by foliage.
SIGF	Foliage cover fraction.
SIGMA	Stefan-Boltzmann constant.
SLOPE1	Part of the root-finding algorithm.
SMALLA	Ground (snowpack) surface absorptivity.
SOL	Calculated solar insolation reaching the top of the foliage layer.
STATE	Arbitrary multiplier (STATE>0) of RS used to account for senescence, stress etc.
SURFGB	Surface (foliage + ground surface) thermal IR emittance, $\text{cal cm}^{-2} \text{min}^{-1}$ .
T1	Temperature at first grid point below surface, distance SRPQ(IX), in TSTM heat transfer algorithm.
TA	Air temperature.
TEFF	Mean effective temperature.
TEFFR	TEFF with reflection incorporated.
TEM1	Ground (snowpack) surface temperature.
TF	Foliage temperature.
TF0	Part of the root-finding algorithm.
TF4	Part of the calculation of FENB.
TG4	Part of the calculation of FENB.
THETAV	Used in the calculation of Richardson's Number.
UA	Wind speed.
UAF	Wind speed of air in the foliage layer.
WET	Moisture content of ground (snowpack) surface.
XL1	$L=f(T_a)$ , used in the calculation of the latent heat of evaporation, a function of air temperature.
XLNGW	Part of the foliage energy-budget calculation.
Z0	Roughness length.
ZA	Instrument height above ground (snowpack).
ZDSP	Zero displacement height.

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